

**HYDROLOGY REPORT**  
for  
**TRACT 38236 & 38237**  
Located in the City of Moreno Valley  
County of Riverside

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## 1. Purpose

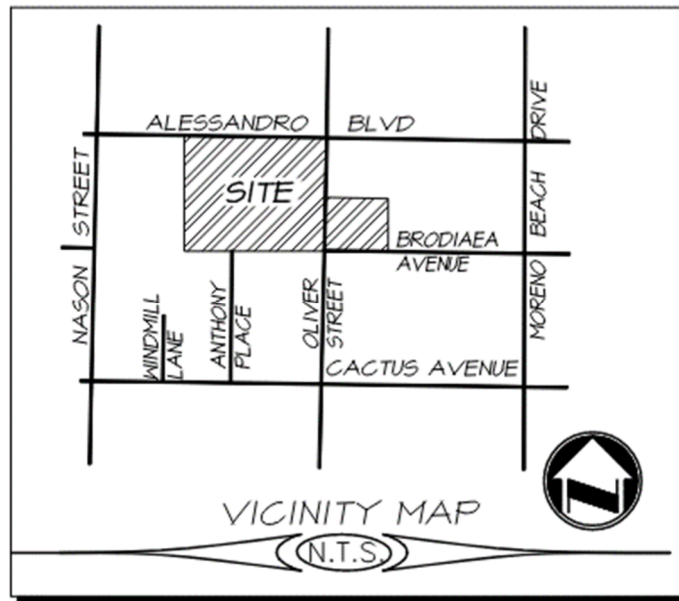
This Hydrology Report has been prepared in order to obtain entitlement approval of Tract 38236. Adkan Engineers has prepared this study to ensure that adequate size and proper operation of drainage facilities are incorporated into the Post-Development project site.

## 2. Project Description

Tract 38236 is located in the City of Moreno Valley north of Brodiaea Avenue, east of Nason Street, south of Alessandro Avenue and west of Oliver Street. The planned development will consist of 204 single-family residences, street improvements, and 4 onsite stormwater treatment areas (Bio-retention basins). They are located South of Lot 70, West of Lot 198, East of Lot 190 and North of Lot 183. Offsite street improvements will be done on Alessandro Avenue and Brodiaea Avenue in order to build out ultimate curb and gutter along the project frontage. All onsite runoff will flow to the south east as per the existing drainage path.

Tract 38237 is located in the City of Moreno Valley north of Brodiaea Avenue, east of Oliver Street, south of Alessandro Avenue and west of Moreno Beach Drive. The planned development will consist of 67 single-family residences, street improvements, and 2 onsite stormwater treatment areas (Bio-retention basins). They are at the intersection of Oliver Street and Brodiaea Avenue and between Lot 47 & 48. Offsite street improvements will be done on Oliver Street and Brodiaea Avenue in order to build out ultimate curb and gutter along the project frontage. All onsite runoff will flow to the south as per the existing drainage path.

## A. Vicinity Map



## 3. Pre-Development Hydrology

Site is vacant with no existing structures or roads on the site. All flows from the site flow towards the south east Existing Q100 runoff flows are shown on the Riverside County Flood Control and Water Conservation District:

Moreno Master Drainage Plan (Adopted October 1980; Revision No.2 April 2015) in Section 3 of this report. Existing Q100 entering MDP Line H at the intersection of Cactus Avenue and Oliver Street drain lines. All major drainage paths along Alessandro Blvd and Brodiaea Avenue are earthen swales. The flows from the swales flow down Oliver Street.

#### 4. Post-Development Hydrology

Tract 38236 Onsite low flow runoff from the proposed development will flow into 4 onsite stormwater treatment areas (Bio-retention basins). They are located South of Lot 70, West of Lot 198, East of Lot 190 and North of Lot 183. Offsite street improvements will be done on Alessandro Avenue and Brodiaea Avenue in order to build out ultimate curb and gutter along the project frontage. All onsite runoff will flow to the south east as per the existing drainage path.

MDP Line H at the intersection of Cactus Avenue and Oliver Street drain lines will be extended towards the intersection of Oliver Street and Brodiaea Avenue to collect the onsite runoff.

Tract 38237 onsite low flow runoff from the proposed development will flow into 2 onsite stormwater treatment areas (Bio-retention basins). They are at the intersection of Oliver Street and Brodiaea Avenue and between Lot 47 & 48. The site drains towards the southeast and the southwest. The east side of the site will flow towards MDP Line H-2 and the west side drains towards the proposed extended MDP Line H.

#### 5. Method of Analysis

The site hydrology was based upon Riverside County Flood Control and Water Conservation District Hydrology Manual, from which pertinent soil and rainfall information was obtained.

Storm flows were determined by the "RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM", Riverside County Flood Control & Water Conservation District 1978 Hydrology Manual, produced by Bondamin Engineering.

#### 6. Summary of Findings

Tract 38236 offsite and onsite flows surrounding the site will be collected by MDP Line H will be adequately sized to convey the 100-year storm event. All onsite flows will be collected by proposed catch basins and storm drain system to pretreat storm flows using the proposed Bio-retention basin prior to discharging into MDP Line H.

Tract 38237 offsite and onsite flows surrounding the site with flow towards the east side of the site will flow towards MDP Line H-2 and the west side drains towards the proposed extended MDP Line H. The extended Line H be adequately sized to convey the 100-year storm event. All onsite flows will be collected by proposed catch basins and storm drain system to pretreat storm flows using the proposed Bio-retention basins in the east and the west prior to discharging into MDP Line H or Line H-2.

Runoff Q's for the proposed storm drain lines on the Moreno Master Drainage Plan (Line H, H-5 &H-5a) are proposed and not existing facilities.

### 7. Conclusion

The hydrologic calculations provided herein substantiate the design of the Post-Development project and indicate the following:

- The Post-Development facilities demonstrate the ability to convey the 100 year storm events

Based on the Hydrology and Hydraulic analysis conducted and results shown herein and part thereof, it is our conclusion this project **does not** negatively impact the local community or watershed goals.



## **Section 1**

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**Post-Development 10 & 100 year Hydrology Offsite & Onsite  
(Rational Method)**





Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro10.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District  
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 10.0  
Calculated rainfall intensity data:  
1 hour intensity = 0.820(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 1.000 to Point/Station 1.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Rainfall intensity = 1.420(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.709  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
User specified values are as follows:  
TC = 20.00 min. Rain intensity = 1.42(In/Hr)  
Total area = 0.00(Ac.) Total runoff = 355.00(CFS)

\*\*\*\*\*  
Process from Point/Station 1.000 to Point/Station 2.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1580.500(Ft.)  
Downstream point/station elevation = 1564.000(Ft.)  
Pipe length = 931.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 355.000(CFS)  
Nearest computed pipe diameter = 60.00(In.)  
Calculated individual pipe flow = 355.000(CFS)  
Normal flow depth in pipe = 50.63(In.)  
Flow top width inside pipe = 43.57(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 20.10(Ft/s)  
Travel time through pipe = 0.77 min.  
Time of concentration (TC) = 20.77 min.

\*\*\*\*\*  
Process from Point/Station 2.000 to Point/Station 2.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 0.000(Ac.)  
Runoff from this stream = 355.000(CFS)  
Time of concentration = 20.77 min.  
Rainfall intensity = 1.394(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 3.000 to Point/Station 4.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 709.000(Ft.)  
Top (of initial area) elevation = 1584.000(Ft.)  
Bottom (of initial area) elevation = 1573.500(Ft.)  
Difference in elevation = 10.500(Ft.)  
Slope = 0.01481 s(percent)= 1.48  
TC = k(0.300)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.622 min.  
Rainfall intensity = 2.048(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.870  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 1.531(CFS)  
Total initial stream area = 0.860(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 4.000 to Point/Station 5.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1573.500(Ft.)  
Downstream point/station elevation = 1569.000(Ft.)  
Pipe length = 65.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.531(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.531(CFS)  
Normal flow depth in pipe = 3.69(In.)  
Flow top width inside pipe = 8.85(In.)  
Critical Depth = 6.84(In.)  
Pipe flow velocity = 8.99(Ft/s)  
Travel time through pipe = 0.12 min.  
Time of concentration (TC) = 9.74 min.

\*\*\*\*\*  
Process from Point/Station 5.000 to Point/Station 5.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 0.860(Ac.)  
Runoff from this stream = 1.531(CFS)  
Time of concentration = 9.74 min.  
Rainfall intensity = 2.035(In/Hr)

\*\*\*\*\*  
Process from Point/Station 6.000 to Point/Station 7.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 370.000(Ft.)  
Top (of initial area) elevation = 1581.300(Ft.)  
Bottom (of initial area) elevation = 1573.500(Ft.)  
Difference in elevation = 7.800(Ft.)  
Slope = 0.02108 s(percent)= 2.11  
TC = k(0.300)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 6.912 min.  
Rainfall intensity = 2.416(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.873  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 0.548(CFS)  
Total initial stream area = 0.260(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 7.000 to Point/Station 5.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1573.500(Ft.)  
Downstream point/station elevation = 1469.000(Ft.)  
Pipe length = 44.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.548(CFS)

Nearest computed pipe diameter = 3.00(In.)  
 Calculated individual pipe flow = 0.548(CFS)  
 Normal flow depth in pipe = 1.32(In.)  
 Flow top width inside pipe = 2.98(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 26.23(Ft/s)  
 Travel time through pipe = 0.03 min.  
 Time of concentration (TC) = 6.94 min.

++++++  
 Process from Point/Station 5.000 to Point/Station 5.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 0.260(Ac.)  
 Runoff from this stream = 0.548(CFS)  
 Time of concentration = 6.94 min.  
 Rainfall intensity = 2.411(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	1.531	9.74	2.035
2	0.548	6.94	2.411

Largest stream flow has longer time of concentration  
 $Q_p = 1.531 + \text{sum of } Q_b \frac{I_a/I_b}{0.548 * 0.844} = 1.994$   
 $Q_p = 1.994$

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 1.531 0.548  
 Area of streams before confluence:  
 0.860 0.260  
 Results of confluence:  
 Total flow rate = 1.994(CFS)  
 Time of concentration = 9.743 min.  
 Effective stream area after confluence = 1.120(Ac.)

++++++  
 Process from Point/Station 5.000 to Point/Station 8.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1569.000(Ft.)  
 Downstream point/station elevation = 1568.300(Ft.)  
 Pipe length = 139.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 1.994(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 1.994(CFS)  
 Normal flow depth in pipe = 8.04(In.)  
 Flow top width inside pipe = 11.29(In.)  
 Critical Depth = 7.23(In.)  
 Pipe flow velocity = 3.57(Ft/s)  
 Travel time through pipe = 0.65 min.  
 Time of concentration (TC) = 10.39 min.

++++++  
 Process from Point/Station 8.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1568.300(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 166.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 2.216(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $\text{Velocity (ft/s)} = (7 + 8(q(\text{English Units})^{0.352})(\text{slope}^{0.5}))$   
 velocity using mean channel flow = 0.75(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0018  
 Corrected/adjusted channel slope = 0.0018  
 Travel time = 3.70 min. TC = 14.09 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.598  
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.692(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.253(CFS) for 0.250(Ac.)  
 Total runoff = 2.247(CFS) Total area = 1.370(Ac.)

+-----+  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 1.370(Ac.)  
 Runoff from this stream = 2.247(CFS)  
 Time of concentration = 14.09 min.  
 Rainfall intensity = 1.692(In/Hr)

+-----+  
 Process from Point/Station 10.000 to Point/Station 11.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 616.000(Ft.)  
 Top (of initial area) elevation = 1579.600(Ft.)  
 Bottom (of initial area) elevation = 1570.300(Ft.)  
 Difference in elevation = 9.300(Ft.)  
 Slope = 0.01510 s(percent) = 1.51  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.779 min.  
 Rainfall intensity = 1.851(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.737  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 3.152(CFS)  
 Total initial stream area = 2.310(Ac.)  
 Pervious area fraction = 0.500

+-----+  
 Process from Point/Station 11.000 to Point/Station 12.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1570.300(Ft.)  
 Downstream point/station elevation = 1568.300(Ft.)  
 Pipe length = 60.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.152(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 3.152(CFS)  
 Normal flow depth in pipe = 5.89(In.)  
 Flow top width inside pipe = 12.00(In.)  
 Critical Depth = 9.12(In.)  
 Pipe flow velocity = 8.22(Ft/s)  
 Travel time through pipe = 0.12 min.  
 Time of concentration (TC) = 11.90 min.

+-----+  
 Process from Point/Station 12.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1568.300(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 161.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 3.152(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{0.5}))$   
 velocity using mean channel flow = 0.82(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0019  
 Corrected/adjusted channel slope = 0.0019  
 Travel time = 3.27 min. TC = 15.18 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea

Runoff Coefficient = 0.591  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.630(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 3.152(CFS) Total area = 2.310(Ac.)

++++++  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 2.310(Ac.)  
 Runoff from this stream = 3.152(CFS)  
 Time of concentration = 15.18 min.  
 Rainfall intensity = 1.630(In/Hr)

++++++  
 Process from Point/Station 7.000 to Point/Station 13.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 207.000(Ft.)  
 Top (of initial area) elevation = 1573.500(Ft.)  
 Bottom (of initial area) elevation = 1570.300(Ft.)  
 Difference in elevation = 3.200(Ft.)  
 Slope = 0.01546 s(percent)= 1.55  
 $TC = k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 5.830 min.  
 Rainfall intensity = 2.631(In/Hr) for a 10.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.874  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.483(CFS)  
 Total initial stream area = 0.210(Ac.)  
 Pervious area fraction = 0.100

++++++  
 Process from Point/Station 13.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1570.300(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 161.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 0.483(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{0.5}))$   
 velocity using mean channel flow = 1.58(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0143  
 Corrected/adjusted channel slope = 0.0143  
 Travel time = 1.70 min. TC = 7.53 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.658  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.314(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 0.483(CFS) Total area = 0.210(Ac.)

++++++  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
Stream flow area = 0.210(Ac.)  
Runoff from this stream = 0.483(CFS)  
Time of concentration = 7.53 min.  
Rainfall intensity = 2.314(In/Hr)

\*\*\*\*\*  
Process from Point/Station 14.000 to Point/Station 15.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 806.000(Ft.)  
Top (of initial area) elevation = 1581.700(Ft.)  
Bottom (of initial area) elevation = 1569.800(Ft.)  
Difference in elevation = 11.900(Ft.)  
Slope = 0.01476 s(percent)= 1.48  
TC =  $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 13.175 min.  
Rainfall intensity = 1.750(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.731  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 3.738(CFS)  
Total initial stream area = 2.920(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 15.000 to Point/Station 16.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1569.800(Ft.)  
Downstream point/station elevation = 1568.300(Ft.)  
Pipe length = 106.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 3.738(CFS)  
Nearest computed pipe diameter = 12.00(In.)  
Calculated individual pipe flow = 3.738(CFS)  
Normal flow depth in pipe = 8.75(In.)  
Flow top width inside pipe = 10.66(In.)  
Critical Depth = 9.87(In.)  
Pipe flow velocity = 6.09(Ft/s)  
Travel time through pipe = 0.29 min.  
Time of concentration (TC) = 13.47 min.

\*\*\*\*\*  
Process from Point/Station 16.000 to Point/Station 9.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1568.300(Ft.)  
End of natural channel elevation = 1568.000(Ft.)  
Length of natural channel = 148.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 3.738(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{0.352})(\text{slope}^{0.5}))$   
Velocity using mean channel flow = 0.89(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0020  
Corrected/adjusted channel slope = 0.0020  
Travel time = 2.78 min. TC = 16.24 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.584  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 1.576(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 3.738(CFS) Total area = 2.920(Ac.)

\*\*\*\*\*  
Process from Point/Station 9.000 to Point/Station 9.000

\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 2 in normal stream number 4  
 Stream flow area = 2.920(Ac.)  
 Runoff from this stream = 3.738(CFS)  
 Time of concentration = 16.24 min.  
 Rainfall intensity = 1.576(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 17.000 to Point/Station 18.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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Initial area flow distance = 483.000(Ft.)  
 Top (of initial area) elevation = 1575.300(Ft.)  
 Bottom (of initial area) elevation = 1570.500(Ft.)  
 Difference in elevation = 4.800(Ft.)  
 Slope = 0.00994 s(percent)= 0.99  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.619 min.  
 Rainfall intensity = 1.863(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.738  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 3.191(CFS)  
 Total initial stream area = 2.320(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 18.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1570.500(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 76.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 3.191(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $Velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{0.5}))$   
 Velocity using mean channel flow = 3.45(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0329  
 Corrected/adjusted channel slope = 0.0329  
 Travel time = 0.37 min. TC = 11.99 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.614  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.835(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 3.191(CFS) Total area = 2.320(Ac.)

\*\*\*\*\*  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 5  
 Stream flow area = 2.320(Ac.)  
 Runoff from this stream = 3.191(CFS)  
 Time of concentration = 11.99 min.  
 Rainfall intensity = 1.835(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	2.247	14.09	1.692
2	3.152	15.18	1.630
3	0.483	7.53	2.314

4            3.738        16.24                    1.576  
 5            3.191        11.99                    1.835  
 Largest stream flow has longer time of concentration  
 Qp =        3.738 + sum of  
           Qb            Ia/Ib  
           2.247 \*        0.931 =        2.093  
           Qb            Ia/Ib  
           3.152 \*        0.967 =        3.047  
           Qb            Ia/Ib  
           0.483 \*        0.681 =        0.329  
           Qb            Ia/Ib  
           3.191 \*        0.859 =        2.741  
 Qp =        11.947  
  
 Total of 5 streams to confluence:  
 Flow rates before confluence point:  
           2.247        3.152        0.483        3.738        3.191  
 Area of streams before confluence:  
           1.370        2.310        0.210        2.920        2.320  
 Results of confluence:  
 Total flow rate =        11.947(CFS)  
 Time of concentration =        16.243 min.  
 Effective stream area after confluence =        9.130(Ac.)

++++++  
 Process from Point/Station            9.000 to Point/Station            2.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1568.000(Ft.)  
 Downstream point/station elevation = 1564.000(Ft.)  
 Pipe length =        53.00(Ft.)    Manning's N = 0.013  
 No. of pipes = 1    Required pipe flow =        11.947(CFS)  
 Nearest computed pipe diameter =        15.00(In.)  
 Calculated individual pipe flow =        11.947(CFS)  
 Normal flow depth in pipe =        9.01(In.)  
 Flow top width inside pipe =        14.69(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity =        15.52(Ft/s)  
 Travel time through pipe =        0.06 min.  
 Time of concentration (TC) =        16.30 min.

++++++  
 Process from Point/Station            2.000 to Point/Station            2.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area =        9.130(Ac.)  
 Runoff from this stream =        11.947(CFS)  
 Time of concentration =        16.30 min.  
 Rainfall intensity =        1.573(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	355.000	20.77	1.394
2	11.947	16.30	1.573

Largest stream flow has longer time of concentration

Qp =        355.000 + sum of  
           Qb            Ia/Ib  
           11.947 \*        0.886 =        10.583  
 Qp =        365.583

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
           355.000        11.947  
 Area of streams before confluence:  
           0.000        9.130  
  
 Results of confluence:  
 Total flow rate =        365.583(CFS)  
 Time of concentration =        20.772 min.  
 Effective stream area after confluence =        9.130(Ac.)

++++++  
 Process from Point/Station            2.000 to Point/Station            19.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length =        861.00(Ft.)    Manning's N = 0.013



No. of pipes = 1 Required pipe flow = 365.583(CFS)  
 Nearest computed pipe diameter = 66.00(In.)  
 Calculated individual pipe flow = 365.583(CFS)  
 Normal flow depth in pipe = 52.03(In.)  
 Flow top width inside pipe = 53.92(In.)  
 Critical Depth = 61.00(In.)  
 Pipe flow velocity = 18.20(Ft/s)  
 Travel time through pipe = 0.79 min.  
 Time of concentration (TC) = 21.56 min.

\*\*\*\*\*  
 Process from Point/Station 19.000 to Point/Station 19.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
 Stream flow area = 9.130(Ac.)  
 Runoff from this stream = 365.583(CFS)  
 Time of concentration = 21.56 min.  
 Rainfall intensity = 1.368(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 18.000 to Point/Station 19.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 662.000(Ft.)  
 Top (of initial area) elevation = 1573.900(Ft.)  
 Bottom (of initial area) elevation = 1567.800(Ft.)  
 Difference in elevation = 6.100(Ft.)  
 Slope = 0.00921 s(percent) = 0.92  
 $TC = k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.294 min.  
 Rainfall intensity = 1.980(In/Hr) for a 10.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.869  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.705(CFS)  
 Total initial stream area = 0.410(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station 19.000 to Point/Station 20.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1567.800(Ft.)  
 End of street segment elevation = 1557.500(Ft.)  
 Length of street segment = 589.000(Ft.)  
 Height of curb above gutter flowline = 6.0(In.)  
 Width of half street (curb to crown) = 18.000(Ft.)  
 Distance from crown to crossfall grade break = 16.000(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 2.000(Ft.)  
 Gutter hike from flowline = 2.000(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 1.030(CFS)  
 Depth of flow = 0.239(Ft.), Average velocity = 2.337(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 5.603(Ft.)  
 Flow velocity = 2.34(Ft/s)  
 Travel time = 4.20 min. TC = 14.49 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.865  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Rainfall intensity = 1.668(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.592(CFS) for 0.410(Ac.)  
 Total runoff = 1.297(CFS) Total area = 0.820(Ac.)

Street flow at end of street = 1.297(CFS)  
Half street flow at end of street = 1.297(CFS)  
Depth of flow = 0.254(Ft.), Average velocity = 2.438(Ft/s)  
Flow width (from curb towards crown)= 6.367(Ft.)

\*\*\*\*\*  
Process from Point/Station 20.000 to Point/Station 21.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1556.500(Ft.)  
Pipe length = 71.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.297(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.297(CFS)  
Normal flow depth in pipe = 5.34(In.)  
Flow top width inside pipe = 8.84(In.)  
Critical Depth = 6.29(In.)  
Pipe flow velocity = 4.75(Ft/s)  
Travel time through pipe = 0.25 min.  
Time of concentration (TC) = 14.74 min.

\*\*\*\*\*  
Process from Point/Station 21.000 to Point/Station 23.000  
\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*

Top of natural channel elevation = 1556.500(Ft.)  
End of natural channel elevation = 1556.000(Ft.)  
Length of natural channel = 38.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 1.479(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.86(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0132  
Corrected/adjusted channel slope = 0.0132  
Travel time = 0.34 min. TC = 15.09 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.592  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 1.635(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.223(CFS) for 0.230(Ac.)  
Total runoff = 1.520(CFS) Total area = 1.050(Ac.)

\*\*\*\*\*  
Process from Point/Station 23.000 to Point/Station 23.000  
\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.050(Ac.)  
Runoff from this stream = 1.520(CFS)  
Time of concentration = 15.09 min.  
Rainfall intensity = 1.635(In/Hr)

\*\*\*\*\*  
Process from Point/Station 13.000 to Point/Station 22.000  
\*\*\* INITIAL AREA EVALUATION \*\*\*

Initial area flow distance = 922.000(Ft.)  
Top (of initial area) elevation = 1570.300(Ft.)  
Bottom (of initial area) elevation = 1557.500(Ft.)  
Difference in elevation = 12.800(Ft.)  
Slope = 0.01388 s(percent)= 1.39  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 10.827 min.  
Rainfall intensity = 1.930(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.868  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 1.274(CFS)  
Total initial stream area = 0.760(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 22.000 to Point/Station 21.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1556.500(Ft.)  
Pipe length = 31.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.274(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.274(CFS)  
Normal flow depth in pipe = 4.12(In.)  
Flow top width inside pipe = 8.97(In.)  
Critical Depth = 6.24(In.)  
Pipe flow velocity = 6.47(Ft/s)  
Travel time through pipe = 0.08 min.  
Time of concentration (TC) = 10.91 min.

\*\*\*\*\*  
Process from Point/Station 21.000 to Point/Station 23.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1556.500(Ft.)  
End of natural channel elevation = 1556.000(Ft.)  
Length of natural channel = 38.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 1.274(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.80(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0132  
Corrected/adjusted channel slope = 0.0132  
Travel time = 0.35 min. TC = 11.26 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.621  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 1.893(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 1.274(CFS) Total area = 0.760(Ac.)

\*\*\*\*\*  
Process from Point/Station 23.000 to Point/Station 23.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
Stream flow area = 0.760(Ac.)  
Runoff from this stream = 1.274(CFS)  
Time of concentration = 11.26 min.  
Rainfall intensity = 1.893(In/Hr)

\*\*\*\*\*  
Process from Point/Station 24.000 to Point/Station 25.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 328.000(Ft.)  
Top (of initial area) elevation = 1570.500(Ft.)  
Bottom (of initial area) elevation = 1566.500(Ft.)  
Difference in elevation = 4.000(Ft.)  
Slope = 0.01220 s(percent) = 1.22  
 $TC = k(0.940)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 23.027 min.  
Rainfall intensity = 1.324(In/Hr) for a 10.0 year storm  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.547  
Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Initial subarea runoff = 0.507(CFS)  
Total initial stream area = 0.700(Ac.)  
Pervious area fraction = 1.000

Process from Point/Station 25.000 to Point/Station 26.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1566.500(Ft.)  
Downstream point/station elevation = 1557.500(Ft.)  
Pipe length = 293.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.507(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 0.507(CFS)  
Normal flow depth in pipe = 3.06(In.)  
Flow top width inside pipe = 6.00(In.)  
Critical Depth = 4.35(In.)  
Pipe flow velocity = 5.05(Ft/s)  
Travel time through pipe = 0.97 min.  
Time of concentration (TC) = 23.99 min.

Process from Point/Station 27.000 to Point/Station 26.000  
\*\*\* SUBAREA FLOW ADDITION \*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.699  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 23.99 min.  
Rainfall intensity = 1.297(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.435(CFS) for 0.480(Ac.)  
Total runoff = 0.942(CFS) Total area = 1.180(Ac.)

Process from Point/Station 26.000 to Point/Station 29.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1557.000(Ft.)  
Pipe length = 39.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.942(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 0.942(CFS)  
Normal flow depth in pipe = 4.52(In.)  
Flow top width inside pipe = 9.00(In.)  
Critical Depth = 5.34(In.)  
Pipe flow velocity = 4.25(Ft/s)  
Travel time through pipe = 0.15 min.  
Time of concentration (TC) = 24.15 min.

Process from Point/Station 30.000 to Point/Station 29.000  
\*\*\* SUBAREA FLOW ADDITION \*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.699  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 24.15 min.  
Rainfall intensity = 1.293(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.614(CFS) for 0.680(Ac.)  
Total runoff = 1.556(CFS) Total area = 1.860(Ac.)

Process from Point/Station 29.000 to Point/Station 32.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1557.000(Ft.)

Downstream point/station elevation = 1556.500(Ft.)  
 Pipe length = 35.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 1.556(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 1.556(CFS)  
 Normal flow depth in pipe = 6.02(In.)  
 Flow top width inside pipe = 8.47(In.)  
 Critical Depth = 6.89(In.)  
 Pipe flow velocity = 4.96(Ft/s)  
 Travel time through pipe = 0.12 min.  
 Time of concentration (TC) = 24.26 min.

\*\*\*\*\*  
 Process from Point/Station 32.000 to Point/Station 23.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1556.500(Ft.)  
 End of natural channel elevation = 1556.000(Ft.)  
 Length of natural channel = 65.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 1.652(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
 Velocity using mean channel flow = 1.45(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0077  
 Corrected/adjusted channel slope = 0.0077  
 Travel time = 0.75 min. TC = 25.01 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.539  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.270(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.157(CFS) for 0.230(Ac.)  
 Total runoff = 1.714(CFS) Total area = 2.090(Ac.)

\*\*\*\*\*  
 Process from Point/Station 23.000 to Point/Station 23.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
 Stream flow area = 2.090(Ac.)  
 Runoff from this stream = 1.714(CFS)  
 Time of concentration = 25.01 min.  
 Rainfall intensity = 1.270(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.520	15.09	1.635
2	1.274	11.26	1.893
3	1.714	25.01	1.270

Largest stream flow has longer time of concentration  
 $Q_p = 1.714 + \text{sum of}$   
 $Q_b \cdot \frac{I_a/I_b}{I_b} = 1.520 * 0.777 = 1.180$   
 $Q_b \cdot \frac{I_a/I_b}{I_b} = 1.274 * 0.671 = 0.855$   
 $Q_p = 3.748$

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 1.520 1.274 1.714  
 Area of streams before confluence:  
 1.050 0.760 2.090

Results of confluence:  
 Total flow rate = 3.748(CFS)  
 Time of concentration = 25.011 min.  
 Effective stream area after confluence = 3.900(Ac.)

\*\*\*\*\*  
 Process from Point/Station 23.000 to Point/Station 19.000

\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1556.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 65.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.748(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 3.748(CFS)  
 Normal flow depth in pipe = 5.93(In.)  
 Flow top width inside pipe = 12.00(In.)  
 Critical Depth = 9.89(In.)  
 Pipe flow velocity = 9.70(Ft/s)  
 Travel time through pipe = 0.11 min.  
 Time of concentration (TC) = 25.12 min.

Process from Point/Station 19.000 to Point/Station 19.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 3.900(Ac.)  
 Runoff from this stream = 3.748(CFS)  
 Time of concentration = 25.12 min.  
 Rainfall intensity = 1.267(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	365.583	21.56	1.368
2	3.748	25.12	1.267

Largest stream flow has longer or shorter time of concentration

Qp = 365.583 + sum of  

$$Q_a \cdot \frac{T_b}{T_a}$$
 3.748 \* 0.858 = 3.217  
 Qp = 368.800

Total of 2 main streams to confluence:

Flow rates before confluence point:

365.583	3.748
Area of streams before confluence:	
9.130	3.900

Results of confluence:

Total flow rate = 368.800(CFS)  
 Time of concentration = 21.561 min.  
 Effective stream area after confluence = 13.030(Ac.)

Process from Point/Station 19.000 to Point/Station 33.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.000(Ft.)  
 Downstream point/station elevation = 1547.000(Ft.)  
 Pipe length = 428.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 368.800(CFS)  
 Nearest computed pipe diameter = 63.00(In.)  
 Calculated individual pipe flow = 368.800(CFS)  
 Normal flow depth in pipe = 55.13(In.)  
 Flow top width inside pipe = 41.67(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 18.37(Ft/s)  
 Travel time through pipe = 0.39 min.  
 Time of concentration (TC) = 21.95 min.

Process from Point/Station 33.000 to Point/Station 33.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
 Stream flow area = 13.030(Ac.)  
 Runoff from this stream = 368.800(CFS)  
 Time of concentration = 21.95 min.  
 Rainfall intensity = 1.356(In/Hr)  
 Program is now starting with Main Stream No. 2

Process from Point/Station 34.000 to Point/Station 35.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 365.000(Ft.)  
 Top (of initial area) elevation = 1566.000(Ft.)  
 Bottom (of initial area) elevation = 1562.000(Ft.)  
 Difference in elevation = 4.000(Ft.)  
 Slope = 0.01096 s(percent)= 1.10  
 $TC = k(0.940)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 24.552 min.  
 Rainfall intensity = 1.282(In/Hr) for a 10.0 year storm  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.541  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Initial subarea runoff = 0.831(CFS)  
 Total initial stream area = 1.200(Ac.)  
 Pervious area fraction = 1.000

---

++++++  
 Process from Point/Station 35.000 to Point/Station 36.000  
 \*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

---

Upstream point/station elevation = 1562.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 329.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.831(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 0.831(CFS)  
 Normal flow depth in pipe = 4.43(In.)  
 Flow top width inside pipe = 5.27(In.)  
 Critical Depth = 5.40(In.)  
 Pipe flow velocity = 5.35(Ft/s)  
 Travel time through pipe = 1.03 min.  
 Time of concentration (TC) = 25.58 min.

---

++++++  
 Process from Point/Station 36.000 to Point/Station 36.000  
 \*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 1.200(Ac.)  
 Runoff from this stream = 0.831(CFS)  
 Time of concentration = 25.58 min.  
 Rainfall intensity = 1.256(In/Hr)

---

++++++  
 Process from Point/Station 59.000 to Point/Station 37.000  
 \*\*\* INITIAL AREA EVALUATION \*\*\*

---

Initial area flow distance = 543.000(Ft.)  
 Top (of initial area) elevation = 1564.500(Ft.)  
 Bottom (of initial area) elevation = 1562.000(Ft.)  
 Difference in elevation = 2.500(Ft.)  
 Slope = 0.00460 s(percent)= 0.46  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 14.202 min.  
 Rainfall intensity = 1.685(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.728  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 2.514(CFS)  
 Total initial stream area = 2.050(Ac.)  
 Pervious area fraction = 0.500

---

++++++  
 Process from Point/Station 37.000 to Point/Station 38.000  
 \*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

---

Upstream point/station elevation = 1562.000(Ft.)  
 Downstream point/station elevation = 1552.000(Ft.)  
 Pipe length = 28.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 2.514(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 2.514(CFS)  
 Normal flow depth in pipe = 3.87(In.)

Flow top width inside pipe = 5.74(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 18.74(Ft/s)  
 Travel time through pipe = 0.02 min.  
 Time of concentration (TC) = 14.23 min.

\*\*\*\*\*  
 Process from Point/Station 62.000 to Point/Station 38.000  
 \*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.727  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Time of concentration = 14.23 min.  
 Rainfall intensity = 1.684(In/Hr) for a 10.0 year storm  
 Subarea runoff = 2.266(CFS) for 1.850(Ac.)  
 Total runoff = 4.780(CFS) Total area = 3.900(Ac.)

\*\*\*\*\*  
 Process from Point/Station 38.000 to Point/Station 36.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1554.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 26.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 4.780(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 4.780(CFS)  
 Normal flow depth in pipe = 7.29(In.)  
 Flow top width inside pipe = 11.72(In.)  
 Critical Depth = 10.85(In.)  
 Pipe flow velocity = 9.58(Ft/s)  
 Travel time through pipe = 0.05 min.  
 Time of concentration (TC) = 14.27 min.

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 36.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 3.900(Ac.)  
 Runoff from this stream = 4.780(CFS)  
 Time of concentration = 14.27 min.  
 Rainfall intensity = 1.681(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.831	25.58	1.256
2	4.780	14.27	1.681

Largest stream flow has longer or shorter time of concentration  
 $Q_p = 4.780 + \text{sum of } \frac{Q_a}{0.831} * \frac{T_b}{0.558} = 0.464$   
 $Q_p = 5.244$

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 0.831 4.780  
 Area of streams before confluence:  
 1.200 3.900  
 Results of confluence:  
 Total flow rate = 5.244(CFS)  
 Time of concentration = 14.272 min.  
 Effective stream area after confluence = 5.100(Ac.)

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 40.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.000(Ft.)  
 Downstream point/station elevation = 1552.500(Ft.)  
 Pipe length = 21.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.244(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 5.244(CFS)



Normal flow depth in pipe = 9.38(In.)  
Flow top width inside pipe = 9.92(In.)  
Critical Depth = 11.15(In.)  
Pipe flow velocity = 7.97(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 14.32 min.

\*\*\*\*\*  
Process from Point/Station 40.000 to Point/Station 41.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1552.500(Ft.)  
End of natural channel elevation = 1552.000(Ft.)  
Length of natural channel = 80.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 5.393(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.70(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0063  
Corrected/adjusted channel slope = 0.0063  
Travel time = 0.79 min. TC = 15.10 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.592  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 1.634(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.280(CFS) for 0.290(Ac.)  
Total runoff = 5.524(CFS) Total area = 5.390(Ac.)

\*\*\*\*\*  
Process from Point/Station 41.000 to Point/Station 41.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 5.390(Ac.)  
Runoff from this stream = 5.524(CFS)  
Time of concentration = 15.10 min.  
Rainfall intensity = 1.634(In/Hr)

\*\*\*\*\*  
Process from Point/Station 55.000 to Point/Station 42.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 657.000(Ft.)  
Top (of initial area) elevation = 1561.600(Ft.)  
Bottom (of initial area) elevation = 1553.000(Ft.)  
Difference in elevation = 8.600(Ft.)  
Slope = 0.01309 s(percent) = 1.31  
 $TC = k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 9.567 min.  
Rainfall intensity = 2.054(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.870  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 1.607(CFS)  
Total initial stream area = 0.900(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 42.000 to Point/Station 43.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.000(Ft.)  
Downstream point/station elevation = 1552.500(Ft.)  
Pipe length = 23.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.607(CFS)

Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 1.607(CFS)  
 Normal flow depth in pipe = 5.33(In.)  
 Flow top width inside pipe = 8.84(In.)  
 Critical Depth = 7.00(In.)  
 Pipe flow velocity = 5.90(Ft/s)  
 Travel time through pipe = 0.07 min.  
 Time of concentration (TC) = 9.63 min.

++++++  
 Process from Point/Station 43.000 to Point/Station 41.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1552.500(Ft.)  
 End of natural channel elevation = 1552.000(Ft.)  
 Length of natural channel = 39.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 1.607(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
 Velocity using mean channel flow = 1.86(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0128  
 Corrected/adjusted channel slope = 0.0128  
 Travel time = 0.35 min. TC = 9.98 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.632  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.011(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 1.607(CFS) Total area = 0.900(Ac.)

++++++  
 Process from Point/Station 41.000 to Point/Station 41.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 0.900(Ac.)  
 Runoff from this stream = 1.607(CFS)  
 Time of concentration = 9.98 min.  
 Rainfall intensity = 2.011(In/Hr)

++++++  
 Process from Point/Station 22.000 to Point/Station 44.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 556.000(Ft.)  
 Top (of initial area) elevation = 1557.500(Ft.)  
 Bottom (of initial area) elevation = 1553.000(Ft.)  
 Difference in elevation = 4.500(Ft.)  
 Slope = 0.00809 s(percent) = 0.81  
 $TC = k(0.300) * [(length^3)/(elevation\ change)]^{.2}$   
 Initial area time of concentration = 9.852 min.  
 Rainfall intensity = 2.024(In/Hr) for a 10.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.869  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.915(CFS)  
 Total initial stream area = 0.520(Ac.)  
 Pervious area fraction = 0.100

++++++  
 Process from Point/Station 44.000 to Point/Station 45.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.000(Ft.)  
 Downstream point/station elevation = 1552.500(Ft.)

Pipe length = 31.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.915(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 0.915(CFS)  
 Normal flow depth in pipe = 4.15(In.)  
 Flow top width inside pipe = 8.97(In.)  
 Critical Depth = 5.25(In.)  
 Pipe flow velocity = 4.59(Ft/s)  
 Travel time through pipe = 0.11 min.  
 Time of concentration (TC) = 9.96 min.

\*\*\*\*\*  
 Process from Point/Station 45.000 to Point/Station 41.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1552.500(Ft.)  
 End of natural channel elevation = 1552.000(Ft.)  
 Length of natural channel = 31.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 0.915(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $Velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{.5}))$   
 velocity using mean channel flow = 1.87(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0161  
 Corrected/adjusted channel slope = 0.0161  
 Travel time = 0.28 min. TC = 10.24 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.630  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.985(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 0.915(CFS) Total area = 0.520(Ac.)

\*\*\*\*\*  
 Process from Point/Station 41.000 to Point/Station 41.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
 Stream flow area = 0.520(Ac.)  
 Runoff from this stream = 0.915(CFS)  
 Time of concentration = 10.24 min.  
 Rainfall intensity = 1.985(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	5.524	15.10	1.634
2	1.607	9.98	2.011
3	0.915	10.24	1.985

Largest stream flow has longer time of concentration

Qp = 5.524 + sum of  
 $Q_b \cdot \frac{I_a}{I_b} = 1.607 * 0.813 = 1.307$   
 $Q_b \cdot \frac{I_a}{I_b} = 0.915 * 0.823 = 0.753$   
 Qp = 7.584

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 5.524 1.607 0.915  
 Area of streams before confluence:  
 5.390 0.900 0.520

Results of confluence:  
 Total flow rate = 7.584(CFS)  
 Time of concentration = 15.102 min.  
 Effective stream area after confluence = 6.810(Ac.)

\*\*\*\*\*  
 Process from Point/Station 41.000 to Point/Station 33.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1552.000(Ft.)  
 Downstream point/station elevation = 1547.000(Ft.)  
 Pipe length = 71.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 7.584(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 7.584(CFS)  
 Normal flow depth in pipe = 8.13(In.)  
 Flow top width inside pipe = 11.22(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 13.38(Ft/s)  
 Travel time through pipe = 0.09 min.  
 Time of concentration (TC) = 15.19 min.

++++++  
 Process from Point/Station 33.000 to Point/Station 33.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 6.810(Ac.)  
 Runoff from this stream = 7.584(CFS)  
 Time of concentration = 15.19 min.  
 Rainfall intensity = 1.630(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	368.800	21.95	1.356
2	7.584	15.19	1.630

Largest stream flow has longer time of concentration

$Q_p = 368.800 + \text{sum of } \frac{Q_b \cdot I_a/I_b}{7.584} = 6.309$   
 $Q_p = 375.109$

Total of 2 main streams to confluence:

Flow rates before confluence point:  
 368.800      7.584  
 Area of streams before confluence:  
 13.030      6.810

Results of confluence:

Total flow rate = 375.109(CFS)  
 Time of concentration = 21.949 min.  
 Effective stream area after confluence = 19.840(Ac.)  
 End of computations, total study area = 19.84 (Ac.)  
 The following figures may be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction( $A_p$ ) = 0.486  
 Area averaged RI index number = 56.7

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro110.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District  
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 10.0  
Calculated rainfall intensity data:  
1 hour intensity = 0.820(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 58.000 to Point/Station 59.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 933.000(Ft.)  
Top (of initial area) elevation = 1575.900(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)  
Difference in elevation = 11.400(Ft.)  
Slope = 0.01222 s(percent)= 1.22  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 14.508 min.  
Rainfall intensity = 1.668(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.726  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 2.871(CFS)  
Total initial stream area = 2.370(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 59.000 to Point/Station 60.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
Downstream point/station elevation = 1561.500(Ft.)  
Pipe length = 22.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.871(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.871(CFS)  
Normal flow depth in pipe = 4.34(In.)  
Flow top width inside pipe = 8.99(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 13.62(Ft/s)  
Travel time through pipe = 0.03 min.  
Time of concentration (TC) = 14.54 min.

\*\*\*\*\*  
Process from Point/Station 60.000 to Point/Station 60.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 2.370(Ac.)

Runoff from this stream = 2.871(CFS)  
 Time of concentration = 14.54 min.  
 Rainfall intensity = 1.666(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 61.000 to Point/Station 62.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 542.000(Ft.)  
 Top (of initial area) elevation = 1572.100(Ft.)  
 Bottom (of initial area) elevation = 1564.500(Ft.)  
 Difference in elevation = 7.600(Ft.)  
 Slope = 0.01402 s(percent)= 1.40  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.358 min.  
 Rainfall intensity = 1.885(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.739  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 1.839(CFS)  
 Total initial stream area = 1.320(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 62.000 to Point/Station 60.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
 Downstream point/station elevation = 1561.500(Ft.)  
 Pipe length = 22.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 1.839(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 1.839(CFS)  
 Normal flow depth in pipe = 4.40(In.)  
 Flow top width inside pipe = 5.31(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 11.92(Ft/s)  
 Travel time through pipe = 0.03 min.  
 Time of concentration (TC) = 11.39 min.

\*\*\*\*\*  
 Process from Point/Station 60.000 to Point/Station 60.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 1.320(Ac.)  
 Runoff from this stream = 1.839(CFS)  
 Time of concentration = 11.39 min.  
 Rainfall intensity = 1.882(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.871	14.54	1.666
2	1.839	11.39	1.882

Largest stream flow has longer time of concentration

Qp = 2.871 + sum of  
 $Qb * \frac{Ia}{Ib}$   
 $1.839 * 0.885 = 1.628$   
 Qp = 4.499

Total of 2 streams to confluence:

Flow rates before confluence point:  
 2.871 1.839

Area of streams before confluence:  
 2.370 1.320

Results of confluence:

Total flow rate = 4.499(CFS)  
 Time of concentration = 14.535 min.  
 Effective stream area after confluence = 3.690(Ac.)

\*\*\*\*\*  
 Process from Point/Station 60.000 to Point/Station 63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.500(Ft.)

Downstream point/station elevation = 1561.000(Ft.)  
Pipe length = 33.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 4.499(CFS)  
Nearest computed pipe diameter = 15.00(In.)  
Calculated individual pipe flow = 4.499(CFS)  
Normal flow depth in pipe = 8.07(In.)  
Flow top width inside pipe = 14.96(In.)  
Critical Depth = 10.31(In.)  
Pipe flow velocity = 6.68(Ft/s)  
Travel time through pipe = 0.08 min.  
Time of concentration (TC) = 14.62 min.

\*\*\*\*\*  
Process from Point/Station 63.000 to Point/Station 63.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
Stream flow area = 3.690(Ac.)  
Runoff from this stream = 4.499(CFS)  
Time of concentration = 14.62 min.  
Rainfall intensity = 1.661(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 64.000 to Point/Station 65.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 888.000(Ft.)  
Top (of initial area) elevation = 1575.100(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)  
Difference in elevation = 10.600(Ft.)  
Slope = 0.01194 s(percent) = 1.19  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 14.291 min.  
Rainfall intensity = 1.680(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.727  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 1.332(CFS)  
Total initial stream area = 1.090(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 65.000 to Point/Station 66.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
Downstream point/station elevation = 1561.500(Ft.)  
Pipe length = 25.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.332(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 1.332(CFS)  
Normal flow depth in pipe = 3.64(In.)  
Flow top width inside pipe = 5.86(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 10.66(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 14.33 min.

\*\*\*\*\*  
Process from Point/Station 66.000 to Point/Station 66.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.090(Ac.)  
Runoff from this stream = 1.332(CFS)  
Time of concentration = 14.33 min.  
Rainfall intensity = 1.678(In/Hr)

\*\*\*\*\*  
Process from Point/Station 67.000 to Point/Station 68.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 776.000(Ft.)  
Top (of initial area) elevation = 1574.100(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)

Difference in elevation = 9.600(Ft.)  
 Slope = 0.01237 s(percent)= 1.24  
 TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.444 min.  
 Rainfall intensity = 1.732(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.730  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 3.998(CFS)  
 Total initial stream area = 3.160(Ac.)  
 Pervious area fraction = 0.500

++++++  
 Process from Point/Station 68.000 to Point/Station 66.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
 Downstream point/station elevation = 1561.500(Ft.)  
 Pipe length = 16.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.998(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 3.998(CFS)  
 Normal flow depth in pipe = 4.80(In.)  
 Flow top width inside pipe = 8.98(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 16.66(Ft/s)  
 Travel time through pipe = 0.02 min.  
 Time of concentration (TC) = 13.46 min.

++++++  
 Process from Point/Station 66.000 to Point/Station 66.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 3.160(Ac.)  
 Runoff from this stream = 3.998(CFS)  
 Time of concentration = 13.46 min.  
 Rainfall intensity = 1.731(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	1.332	14.33	1.678
2	3.998	13.46	1.731

Largest stream flow has longer or shorter time of concentration

Qp = 3.998 + sum of  
 $Qa \cdot \frac{Tb}{Ta}$   
 $1.332 * 0.939 = 1.251$   
 Qp = 5.249

Total of 2 streams to confluence:

Flow rates before confluence point:

1.332	3.998
-------	-------

Area of streams before confluence:

1.090	3.160
-------	-------

Results of confluence:

Total flow rate = 5.249(CFS)  
 Time of concentration = 13.460 min.  
 Effective stream area after confluence = 4.250(Ac.)

++++++  
 Process from Point/Station 66.000 to Point/Station 63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.500(Ft.)  
 Downstream point/station elevation = 1561.000(Ft.)  
 Pipe length = 25.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.249(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 5.249(CFS)  
 Normal flow depth in pipe = 8.16(In.)  
 Flow top width inside pipe = 14.94(In.)  
 Critical Depth = 11.14(In.)  
 Pipe flow velocity = 7.70(Ft/s)  
 Travel time through pipe = 0.05 min.  
 Time of concentration (TC) = 13.51 min.



+-----+  
 Process from Point/Station 63.000 to Point/Station 63.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 4.250(Ac.)  
 Runoff from this stream = 5.249(CFS)  
 Time of concentration = 13.51 min.  
 Rainfall intensity = 1.728(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	4.499	14.62	1.661
2	5.249	13.51	1.728

Largest stream flow has longer or shorter time of concentration

Qp = 5.249 + sum of  

$$Q_a \cdot \frac{T_b}{T_a}$$
 Qp = 4.499 \* 0.925 = 4.159  
 9.408

Total of 2 main streams to confluence:

Flow rates before confluence point:

4.499 5.249

Area of streams before confluence:

3.690 4.250

Results of confluence:

Total flow rate = 9.408(CFS)

Time of concentration = 13.514 min.

Effective stream area after confluence = 7.940(Ac.)

+-----+  
 Process from Point/Station 63.000 to Point/Station 69.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.000(Ft.)  
 Downstream point/station elevation = 1560.500(Ft.)  
 Pipe length = 91.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 9.408(CFS)  
 Nearest computed pipe diameter = 21.00(In.)  
 Calculated individual pipe flow = 9.408(CFS)  
 Normal flow depth in pipe = 14.23(In.)  
 Flow top width inside pipe = 19.63(In.)  
 Critical depth = 13.70(In.)  
 Pipe flow velocity = 5.43(Ft/s)  
 Travel time through pipe = 0.28 min.  
 Time of concentration (TC) = 13.79 min.

+-----+  
 Process from Point/Station 69.000 to Point/Station 57.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1560.500(Ft.)  
 End of natural channel elevation = 1560.000(Ft.)  
 Length of natural channel = 113.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 9.722(CFS)

Natural valley channel type used

L.A. County flood control district formula for channel velocity:

Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{0.352})(\text{slope}^{0.5}))$

Velocity using mean channel flow = 1.65(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)

Normal channel slope = 0.0044

Corrected/adjusted channel slope = 0.0044

Travel time = 1.14 min. TC = 14.93 min.

Adding area flow to channel

UNDEVELOPED (good cover) subarea

Runoff Coefficient = 0.593

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

RI index for soil(AMC 2) = 61.00

Pervious area fraction = 1.000; Impervious fraction = 0.000

Rainfall intensity = 1.644(In/Hr) for a 10.0 year storm

Subarea runoff = 0.516(CFS) for 0.530(Ac.)  
Total runoff = 9.925(CFS) Total area = 8.470(Ac.)

\*\*\*\*\*  
Process from Point/Station 57.000 to Point/Station 57.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 8.470(Ac.)  
Runoff from this stream = 9.925(CFS)  
Time of concentration = 14.93 min.  
Rainfall intensity = 1.644(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 6.000 to Point/Station 54.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 873.000(Ft.)  
Top (of initial area) elevation = 1581.300(Ft.)  
Bottom (of initial area) elevation = 1573.000(Ft.)  
Difference in elevation = 8.300(Ft.)  
Slope = 0.00951 s(percent)= 0.95  
TC =  $k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 11.427 min.  
Rainfall intensity = 1.879(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.868  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 2.071(CFS)  
Total initial stream area = 1.270(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 54.000 to Point/Station 55.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1573.000(Ft.)  
End of street segment elevation = 1561.600(Ft.)  
Length of street segment = 542.000(Ft.)  
Height of curb above gutter flowline = 6.0(In.)  
width of half street (curb to crown) = 32.000(Ft.)  
Distance from crown to crossfall grade break = 30.000(Ft.)  
Slope from gutter to grade break (v/hz) = 0.020  
Slope from grade break to crown (v/hz) = 0.020  
Street flow is on [1] side(s) of the street  
Distance from curb to property line = 18.000(Ft.)  
Slope from curb to property line (v/hz) = 0.020  
Gutter width = 2.000(Ft.)  
Gutter hike from flowline = 2.000(In.)  
Manning's N in gutter = 0.0150  
Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 3.060(CFS)  
Depth of flow = 0.311(Ft.), Average velocity = 3.142(Ft/s)  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 9.204(Ft.)  
Flow velocity = 3.14(Ft/s)  
Travel time = 2.88 min. TC = 14.30 min.  
Adding area flow to street  
COMMERCIAL subarea type  
Runoff Coefficient = 0.865  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Rainfall intensity = 1.680(In/Hr) for a 10.0 year storm  
Subarea runoff = 1.919(CFS) for 1.320(Ac.)  
Total runoff = 3.990(CFS) Total area = 2.590(Ac.)  
Street flow at end of street = 3.990(CFS)  
Half street flow at end of street = 3.990(CFS)  
Depth of flow = 0.333(Ft.), Average velocity = 3.337(Ft/s)  
Flow width (from curb towards crown)= 10.339(Ft.)

\*\*\*\*\*

Process from Point/Station 55.000 to Point/Station 56.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.600(Ft.)  
 Downstream point/station elevation = 1560.500(Ft.)  
 Pipe length = 159.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.990(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 3.990(CFS)  
 Normal flow depth in pipe = 9.62(In.)  
 Flow top width inside pipe = 14.39(In.)  
 Critical Depth = 9.69(In.)  
 Pipe flow velocity = 4.79(Ft/s)  
 Travel time through pipe = 0.55 min.  
 Time of concentration (TC) = 14.85 min.

\*\*\*\*\*  
 Process from Point/Station 56.000 to Point/Station 57.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1560.500(Ft.)  
 End of natural channel elevation = 1560.000(Ft.)  
 Length of natural channel = 90.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 3.990(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
 Velocity using mean channel flow = 1.49(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0056  
 Corrected/adjusted channel slope = 0.0056  
 Travel time = 1.01 min. TC = 15.86 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.587  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.595(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 3.990(CFS) Total area = 2.590(Ac.)

\*\*\*\*\*  
 Process from Point/Station 57.000 to Point/Station 53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 104.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.990(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 3.990(CFS)  
 Normal flow depth in pipe = 5.76(In.)  
 Flow top width inside pipe = 11.99(In.)  
 Critical Depth = 10.15(In.)  
 Pipe flow velocity = 10.71(Ft/s)  
 Travel time through pipe = 0.16 min.  
 Time of concentration (TC) = 16.02 min.

\*\*\*\*\*  
 Process from Point/Station 57.000 to Point/Station 57.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 2.590(Ac.)  
 Runoff from this stream = 3.990(CFS)  
 Time of concentration = 16.02 min.  
 Rainfall intensity = 1.587(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	9.925	14.93	1.644

2            3.990        16.02                    1.587  
 Largest stream flow has longer or shorter time of concentration  
 $Q_p = 9.925 + \text{sum of}$   
 $Q_a \quad T_b/T_a$   
 $3.990 * 0.932 = 3.719$   
 $Q_p = 13.643$

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
           9.925            3.990  
 Area of streams before confluence:  
           8.470            2.590

Results of confluence:  
 Total flow rate = 13.643(CFS)  
 Time of concentration = 14.934 min.  
 Effective stream area after confluence = 11.060(Ac.)

\*\*\*\*\*  
 Process from Point/Station        57.000 to Point/Station        53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 104.00(Ft.)    Manning's N = 0.013  
 No. of pipes = 1    Required pipe flow = 13.643(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 13.643(CFS)  
 Normal flow depth in pipe = 10.92(In.)  
 Flow top width inside pipe = 13.35(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 14.27(Ft/s)  
 Travel time through pipe = 0.12 min.  
 Time of concentration (TC) = 15.06 min.

\*\*\*\*\*  
 Process from Point/Station        53.000 to Point/Station        53.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:  
 In Main Stream number: 1  
 Stream flow area = 11.060(Ac.)  
 Runoff from this stream = 13.643(CFS)  
 Time of concentration = 15.06 min.  
 Rainfall intensity = 1.637(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station        51.000 to Point/Station        52.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 664.000(Ft.)  
 Top (of initial area) elevation = 14574.500(Ft.)  
 Bottom (of initial area) elevation = 1560.000(Ft.)  
 Difference in elevation = 13014.500(Ft.)  
 Slope = 19.60015 s(percent) = 1960.02  
 $TC = k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
 Warning: TC computed to be less than 5 min.; program is assuming the  
 time of concentration is 5 minutes.  
 Initial area time of concentration = 5.000 min.  
 Rainfall intensity = 2.841(In/Hr) for a 10.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.876  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 5.921(CFS)  
 Total initial stream area = 2.380(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station        52.000 to Point/Station        53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 250.00(Ft.)    Manning's N = 0.015  
 No. of pipes = 1    Required pipe flow = 5.921(CFS)  
 Nearest computed pipe diameter = 15.00(In.)

Calculated individual pipe flow = 5.921(CFS)  
 Normal flow depth in pipe = 9.09(In.)  
 Flow top width inside pipe = 14.66(In.)  
 Critical Depth = 11.81(In.)  
 Pipe flow velocity = 7.61(Ft/s)  
 Travel time through pipe = 0.55 min.  
 Time of concentration (TC) = 5.55 min.

\*\*\*\*\*  
 Process from Point/Station 53.000 to Point/Station 53.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 2.380(Ac.)  
 Runoff from this stream = 5.921(CFS)  
 Time of concentration = 5.55 min.  
 Rainfall intensity = 2.697(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	13.643	15.06	1.637
2	5.921	5.55	2.697

Largest stream flow has longer time of concentration

Qp = 13.643 + sum of  

$$Q_b \frac{I_a/I_b}{5.921 * 0.607} = 3.594$$
  
 Qp = 17.237

Total of 2 main streams to confluence:

Flow rates before confluence point:  
 13.643 5.921  
 Area of streams before confluence:  
 11.060 2.380

Results of confluence:

Total flow rate = 17.237(CFS)  
 Time of concentration = 15.056 min.  
 Effective stream area after confluence = 13.440(Ac.)

\*\*\*\*\*  
 Process from Point/Station 53.000 to Point/Station 70.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1554.000(Ft.)  
 Downstream point/station elevation = 1546.000(Ft.)  
 Pipe length = 416.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 17.237(CFS)  
 Nearest computed pipe diameter = 21.00(In.)  
 Calculated individual pipe flow = 17.237(CFS)  
 Normal flow depth in pipe = 14.02(In.)  
 Flow top width inside pipe = 19.79(In.)  
 Critical Depth = 18.23(In.)  
 Pipe flow velocity = 10.11(Ft/s)  
 Travel time through pipe = 0.69 min.  
 Time of concentration (TC) = 15.74 min.

\*\*\*\*\*  
 Process from Point/Station 70.000 to Point/Station 70.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
 Stream flow area = 13.440(Ac.)  
 Runoff from this stream = 17.237(CFS)  
 Time of concentration = 15.74 min.  
 Rainfall intensity = 1.601(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 71.000 to Point/Station 72.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 424.000(Ft.)  
 Top (of initial area) elevation = 1562.000(Ft.)  
 Bottom (of initial area) elevation = 1553.800(Ft.)  
 Difference in elevation = 8.200(Ft.)  
 Slope = 0.01934 s(percent) = 1.93  
 $TC = k(0.390) * [(length^3)/(elevation change)]^{0.2}$

Initial area time of concentration = 9.654 min.  
Rainfall intensity = 2.044(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.748  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 1.620(CFS)  
Total initial stream area = 1.060(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 72.000 to Point/Station 73.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.800(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 20.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.620(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 1.620(CFS)  
Normal flow depth in pipe = 3.57(In.)  
Flow top width inside pipe = 5.89(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 13.32(Ft/s)  
Travel time through pipe = 0.03 min.  
Time of concentration (TC) = 9.68 min.

\*\*\*\*\*  
Process from Point/Station 73.000 to Point/Station 73.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.060(Ac.)  
Runoff from this stream = 1.620(CFS)  
Time of concentration = 9.68 min.  
Rainfall intensity = 2.042(In/Hr)

\*\*\*\*\*  
Process from Point/Station 74.000 to Point/Station 75.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 318.000(Ft.)  
Top (of initial area) elevation = 1562.000(Ft.)  
Bottom (of initial area) elevation = 1553.800(Ft.)  
Difference in elevation = 8.200(Ft.)  
Slope = 0.02579 s(percent)= 2.58  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 8.124 min.  
Rainfall intensity = 2.228(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.756  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 2.696(CFS)  
Total initial stream area = 1.600(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 75.000 to Point/Station 73.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.800(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 29.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.696(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.696(CFS)  
Normal flow depth in pipe = 4.23(In.)  
Flow top width inside pipe = 8.98(In.)  
Critical Depth = 8.46(In.)  
Pipe flow velocity = 13.20(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 8.16 min.

\*\*\*\*\*  
 Process from Point/Station 73.000 to Point/Station 73.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 1.600(Ac.)  
 Runoff from this stream = 2.696(CFS)  
 Time of concentration = 8.16 min.  
 Rainfall intensity = 2.223(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	1.620	9.68	2.042
2	2.696	8.16	2.223

Largest stream flow has longer or shorter time of concentration

Qp = 2.696 + sum of  
 Qa Tb/Ta  
 1.620 \* 0.843 = 1.366  
 Qp = 4.062

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 1.620 2.696

Area of streams before confluence:  
 1.060 1.600

Results of confluence:  
 Total flow rate = 4.062(CFS)  
 Time of concentration = 8.160 min.  
 Effective stream area after confluence = 2.660(Ac.)

\*\*\*\*\*  
 Process from Point/Station 73.000 to Point/Station 76.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.000(Ft.)  
 Downstream point/station elevation = 1549.000(Ft.)  
 Pipe length = 152.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 4.062(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 4.062(CFS)  
 Normal flow depth in pipe = 9.91(In.)  
 Flow top width inside pipe = 14.20(In.)  
 Critical Depth = 9.79(In.)  
 Pipe flow velocity = 4.72(Ft/s)  
 Travel time through pipe = 0.54 min.  
 Time of concentration (TC) = 8.70 min.

\*\*\*\*\*  
 Process from Point/Station 76.000 to Point/Station 76.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 2.660(Ac.)  
 Runoff from this stream = 4.062(CFS)  
 Time of concentration = 8.70 min.  
 Rainfall intensity = 2.154(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 52.000 to Point/Station 76.500  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 347.000(Ft.)  
 Top (of initial area) elevation = 1560.000(Ft.)  
 Bottom (of initial area) elevation = 1555.500(Ft.)  
 Difference in elevation = 4.500(Ft.)  
 Slope = 0.01297 s(percent) = 1.30  
 $TC = k(0.390) * [(length^3)/(elevation change)]^{0.2}$   
 Initial area time of concentration = 9.652 min.  
 Rainfall intensity = 2.044(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.748  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 0.611(CFS)  
 Total initial stream area = 0.400(Ac.)  
 Pervious area fraction = 0.500

Process from Point/Station 76.500 to Point/Station 76.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1555.500(Ft.)  
 Downstream point/station elevation = 1549.000(Ft.)  
 Pipe length = 70.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.611(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 0.611(CFS)  
 Normal flow depth in pipe = 2.48(In.)  
 Flow top width inside pipe = 5.91(In.)  
 Critical Depth = 4.77(In.)  
 Pipe flow velocity = 7.98(Ft/s)  
 Travel time through pipe = 0.15 min.  
 Time of concentration (TC) = 9.80 min.

Process from Point/Station 76.000 to Point/Station 76.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 0.400(Ac.)  
 Runoff from this stream = 0.611(CFS)  
 Time of concentration = 9.80 min.  
 Rainfall intensity = 2.029(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	4.062	8.70	2.154
2	0.611	9.80	2.029

Largest stream flow has longer or shorter time of concentration

Qp = 4.062 + sum of  

$$Q_a \frac{T_b}{T_a}$$
 0.611 \* 0.888 = 0.543  
 Qp = 4.604

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 4.062 0.611  
 Area of streams before confluence:  
 2.660 0.400  
 Results of confluence:  
 Total flow rate = 4.604(CFS)  
 Time of concentration = 8.698 min.  
 Effective stream area after confluence = 3.060(Ac.)

Process from Point/Station 76.000 to Point/Station 77.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1549.000(Ft.)  
 Downstream point/station elevation = 1548.000(Ft.)  
 Pipe length = 146.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 4.604(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 4.604(CFS)  
 Normal flow depth in pipe = 10.73(In.)  
 Flow top width inside pipe = 13.53(In.)  
 Critical Depth = 10.44(In.)  
 Pipe flow velocity = 4.90(Ft/s)  
 Travel time through pipe = 0.50 min.  
 Time of concentration (TC) = 9.19 min.

Process from Point/Station 77.000 to Point/Station 78.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
 End of natural channel elevation = 1547.500(Ft.)  
 Length of natural channel = 77.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 4.860(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  

$$\text{Velocity(ft/s)} = (7 + 8(q(\text{English Units})^{0.352})(\text{slope}^{0.5}))$$
 velocity using mean channel flow = 1.69(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)



Normal channel slope = 0.0065  
Corrected/adjusted channel slope = 0.0065  
Travel time = 0.76 min. TC = 9.95 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.632  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.013(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.433(CFS) for 0.340(Ac.)  
Total runoff = 5.037(CFS) Total area = 3.400(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 3.400(Ac.)  
Runoff from this stream = 5.037(CFS)  
Time of concentration = 9.95 min.  
Rainfall intensity = 2.013(In/Hr)

\*\*\*\*\*  
Process from Point/Station 79.000 to Point/Station 80.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 227.000(Ft.)  
Top (of initial area) elevation = 1555.200(Ft.)  
Bottom (of initial area) elevation = 1552.500(Ft.)  
Difference in elevation = 2.700(Ft.)  
Slope = 0.01189 s(percent) = 1.19  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 8.287 min.  
Rainfall intensity = 2.206(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.755  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 1.333(CFS)  
Total initial stream area = 0.800(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 80.000 to Point/Station 81.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1552.500(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 22.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.333(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 1.333(CFS)  
Normal flow depth in pipe = 3.71(In.)  
Flow top width inside pipe = 5.83(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 10.44(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 8.32 min.

\*\*\*\*\*  
Process from Point/Station 82.000 to Point/Station 81.000  
\*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

---

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.755  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 8.32 min.  
Rainfall intensity = 2.202(In/Hr) for a 10.0 year storm

Subarea runoff = 1.263(CFS) for 0.760(Ac.)  
Total runoff = 2.596(CFS) Total area = 1.560(Ac.)

\*\*\*\*\*  
Process from Point/Station 81.000 to Point/Station 84.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.000(Ft.)  
Downstream point/station elevation = 1548.000(Ft.)  
Pipe length = 230.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.596(CFS)  
Nearest computed pipe diameter = 12.00(In.)  
Calculated individual pipe flow = 2.596(CFS)  
Normal flow depth in pipe = 7.98(In.)  
Flow top width inside pipe = 11.33(In.)  
Critical Depth = 8.28(In.)  
Pipe flow velocity = 4.68(Ft/s)  
Travel time through pipe = 0.82 min.  
Time of concentration (TC) = 9.14 min.

\*\*\*\*\*  
Process from Point/Station 84.000 to Point/Station 78.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
End of natural channel elevation = 1547.500(Ft.)  
Length of natural channel = 74.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 2.596(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$   
Velocity using mean channel flow = 1.50(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0068  
Corrected/adjusted channel slope = 0.0068  
Travel time = 0.82 min. TC = 9.97 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.632  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.012(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 2.596(CFS) Total area = 1.560(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
Stream flow area = 1.560(Ac.)  
Runoff from this stream = 2.596(CFS)  
Time of concentration = 9.97 min.  
Rainfall intensity = 2.012(In/Hr)

\*\*\*\*\*  
Process from Point/Station 85.000 to Point/Station 86.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 189.000(Ft.)  
Top (of initial area) elevation = 1553.500(Ft.)  
Bottom (of initial area) elevation = 1553.000(Ft.)  
Difference in elevation = 0.500(Ft.)  
Slope = 0.00265 s(percent) = 0.26  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 8.002 min.  
Rainfall intensity = 2.245(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.871  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00

Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 0.333(CFS)  
Total initial stream area = 0.170(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 86.000 to Point/Station 87.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.000(Ft.)  
Downstream point/station elevation = 1548.000(Ft.)  
Pipe length = 34.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.333(CFS)  
Nearest computed pipe diameter = 3.00(In.)  
Calculated individual pipe flow = 0.333(CFS)  
Normal flow depth in pipe = 2.41(In.)  
Flow top width inside pipe = 2.39(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 7.87(Ft/s)  
Travel time through pipe = 0.07 min.  
Time of concentration (TC) = 8.07 min.

\*\*\*\*\*  
Process from Point/Station 87.000 to Point/Station 78.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
End of natural channel elevation = 1547.500(Ft.)  
Length of natural channel = 23.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 0.333(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.83(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0217  
Corrected/adjusted channel slope = 0.0217  
Travel time = 0.21 min. TC = 8.28 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.649  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.207(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 0.333(CFS) Total area = 0.170(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
Stream flow area = 0.170(Ac.)  
Runoff from this stream = 0.333(CFS)  
Time of concentration = 8.28 min.  
Rainfall intensity = 2.207(In/Hr)

\*\*\*\*\*  
Process from Point/Station 76.500 to Point/Station 88.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 248.000(Ft.)  
Top (of initial area) elevation = 1555.500(Ft.)  
Bottom (of initial area) elevation = 1553.500(Ft.)  
Difference in elevation = 2.000(Ft.)  
Slope = 0.00806 s(percent)= 0.81  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 7.138 min.  
Rainfall intensity = 2.377(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.872  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.664(CFS)  
 Total initial stream area = 0.320(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station 88.000 to Point/Station 89.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.500(Ft.)  
 Downstream point/station elevation = 1548.000(Ft.)  
 Pipe length = 37.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.664(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 0.664(CFS)  
 Normal flow depth in pipe = 2.28(In.)  
 Flow top width inside pipe = 5.83(In.)  
 Critical Depth = 4.95(In.)  
 Pipe flow velocity = 9.69(Ft/s)  
 Travel time through pipe = 0.06 min.  
 Time of concentration (TC) = 7.20 min.

\*\*\*\*\*  
 Process from Point/Station 89.000 to Point/Station 78.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
 End of natural channel elevation = 1547.500(Ft.)  
 Length of natural channel = 5.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 0.664(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) = (7 + 8(q(English units)<sup>0.352</sup>)(slope<sup>0.5</sup>)  
 Velocity using mean channel flow = 4.40(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.1000  
 Corrected/adjusted channel slope = 0.1000  
 Travel time = 0.02 min. TC = 7.22 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.661  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.364(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 0.664(CFS) Total area = 0.320(Ac.)

\*\*\*\*\*  
 Process from Point/Station 78.000 to Point/Station 78.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 4  
 Stream flow area = 0.320(Ac.)  
 Runoff from this stream = 0.664(CFS)  
 Time of concentration = 7.22 min.  
 Rainfall intensity = 2.364(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	5.037	9.95	2.013
2	2.596	9.97	2.012
3	0.333	8.28	2.207
4	0.664	7.22	2.364

Largest stream flow has longer or shorter time of concentration  
 Qp = 5.037 + sum of  
 Qa Tb/Ta  
 2.596 \* 0.999 = 2.593  
 Qb Ia/Ib  
 0.333 \* 0.912 = 0.303  
 Qb Ia/Ib

Qp = 0.664 \* 0.852 = 0.565  
 8.499

Total of 4 streams to confluence:  
 Flow rates before confluence point:  
 5.037 2.596 0.333 0.664  
 Area of streams before confluence:  
 3.400 1.560 0.170 0.320  
 Results of confluence:  
 Total flow rate = 8.499(CFS)  
 Time of concentration = 9.954 min.  
 Effective stream area after confluence = 5.450(Ac.)

\*\*\*\*\*  
 Process from Point/Station 78.000 to Point/Station 70.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1547.500(Ft.)  
 Downstream point/station elevation = 1546.000(Ft.)  
 Pipe length = 79.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 8.499(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 8.499(CFS)  
 Normal flow depth in pipe = 11.72(In.)  
 Flow top width inside pipe = 12.40(In.)  
 Critical Depth = 13.64(In.)  
 Pipe flow velocity = 8.26(Ft/s)  
 Travel time through pipe = 0.16 min.  
 Time of concentration (TC) = 10.11 min.

\*\*\*\*\*  
 Process from Point/Station 70.000 to Point/Station 70.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 5.450(Ac.)  
 Runoff from this stream = 8.499(CFS)  
 Time of concentration = 10.11 min.  
 Rainfall intensity = 1.997(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	17.237	15.74	1.601
2	8.499	10.11	1.997

Largest stream flow has longer time of concentration

Qp = 17.237 + sum of  
 Qb Ia/Ib  
 8.499 \* 0.802 = 6.812  
 Qp = 24.049

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
 17.237 8.499  
 Area of streams before confluence:  
 13.440 5.450

Results of confluence:  
 Total flow rate = 24.049(CFS)  
 Time of concentration = 15.741 min.  
 Effective stream area after confluence = 18.890(Ac.)

\*\*\*\*\*  
 Process from Point/Station 70.000 to Point/Station 50.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1546.000(Ft.)  
 Downstream point/station elevation = 1545.000(Ft.)  
 Pipe length = 25.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 24.049(CFS)  
 Nearest computed pipe diameter = 21.00(In.)  
 Calculated individual pipe flow = 24.049(CFS)  
 Normal flow depth in pipe = 13.69(In.)  
 Flow top width inside pipe = 20.01(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 14.49(Ft/s)  
 Travel time through pipe = 0.03 min.  
 Time of concentration (TC) = 15.77 min.

\*\*\*\*\*  
 Process from Point/Station 50.000 to Point/Station 50.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 1  
 Stream flow area = 18.890(Ac.)  
 Runoff from this stream = 24.049(CFS)  
 Time of concentration = 15.77 min.  
 Rainfall intensity = 1.599(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 33.000 to Point/Station 50.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Rainfall intensity = 1.365(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.705  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 User specified values are as follows:  
 TC = 21.65 min. Rain intensity = 1.37(In/Hr)  
 Total area = 19.85(Ac.) Total runoff = 375.11(CFS)

\*\*\*\*\*  
 Process from Point/Station 50.000 to Point/Station 50.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 19.850(Ac.)  
 Runoff from this stream = 375.110(CFS)  
 Time of concentration = 21.65 min.  
 Rainfall intensity = 1.365(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	24.049	15.77	1.599
2	375.110	21.65	1.365

Largest stream flow has longer time of concentration  
 $Q_p = 375.110 + \text{sum of } \frac{Q_b \cdot I_a/I_b}{24.049} = 395.636$

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
 24.049 375.110  
 Area of streams before confluence:  
 18.890 19.850

Results of confluence:  
 Total flow rate = 395.636(CFS)  
 Time of concentration = 21.650 min.  
 Effective stream area after confluence = 38.740(Ac.)  
 End of computations, total study area = 38.74 (Ac.)  
 The following figures may be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.455  
 Area averaged RI index number = 56.1

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro210.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District 1978 hydrology manual  
Storm event (year) = 10.00 Antecedent Moisture Condition = 2  
Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)  
Storm event year = 10.0  
Calculated rainfall intensity data:  
1 hour intensity = 0.820(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 51.000 to Point/Station 100.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 462.000(Ft.)  
Top (of initial area) elevation = 1574.500(Ft.)  
Bottom (of initial area) elevation = 1570.800(Ft.)  
Difference in elevation = 3.700(Ft.)  
Slope = 0.00801 s(percent)= 0.80  
TC = k(0.300)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.168 min.  
Rainfall intensity = 2.098(In/Hr) for a 10.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.870  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 2.281(CFS)  
Total initial stream area = 1.250(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 100.000 to Point/Station 101.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1570.800(Ft.)  
End of natural channel elevation = 1559.000(Ft.)  
Length of natural channel = 604.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 8.259(CFS)  
Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)  
Velocity using mean channel flow = 3.33(Ft/s)  
Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0195  
Corrected/adjusted channel slope = 0.0195  
Travel time = 3.02 min. TC = 12.19 min.  
Adding area flow to channel  
COMMERCIAL subarea type  
Runoff Coefficient = 0.867  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Rainfall intensity = 1.819(In/Hr) for a 10.0 year storm  
Subarea runoff = 10.332(CFS) for 6.550(Ac.)  
Total runoff = 12.613(CFS) Total area = 7.800(Ac.)

\*\*\*\*\*  
Process from Point/Station 101.000 to Point/Station 101.000  
\*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

---

UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.613  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Time of concentration = 12.19 min.  
Rainfall intensity = 1.819(In/Hr) for a 10.0 year storm  
Subarea runoff = 0.502(CFS) for 0.450(Ac.)  
Total runoff = 13.115(CFS) Total area = 8.250(Ac.)

\*\*\*\*\*  
Process from Point/Station 101.000 to Point/Station 102.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1559.000(Ft.)  
Downstream point/station elevation = 1549.500(Ft.)  
Pipe length = 695.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 13.115(CFS)  
Nearest computed pipe diameter = 21.00(In.)  
Calculated individual pipe flow = 13.115(CFS)  
Normal flow depth in pipe = 13.04(In.)  
Flow top width inside pipe = 20.37(In.)  
Critical Depth = 16.18(In.)  
Pipe flow velocity = 8.35(Ft/s)  
Travel time through pipe = 1.39 min.  
Time of concentration (TC) = 13.58 min.

\*\*\*\*\*  
Process from Point/Station 102.000 to Point/Station 102.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 8.250(Ac.)  
Runoff from this stream = 13.115(CFS)  
Time of concentration = 13.58 min.  
Rainfall intensity = 1.724(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 103.000 to Point/Station 104.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 551.000(Ft.)  
Top (of initial area) elevation = 1558.000(Ft.)  
Bottom (of initial area) elevation = 1552.000(Ft.)  
Difference in elevation = 6.000(Ft.)  
Slope = 0.01089 s(percent)= 1.09  
TC =  $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 12.026 min.  
Rainfall intensity = 1.832(In/Hr) for a 10.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.736  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 3.169(CFS)  
Total initial stream area = 2.350(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 104.000 to Point/Station 105.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1552.000(Ft.)  
Downstream point/station elevation = 1550.500(Ft.)  
Pipe length = 34.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 3.169(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 3.169(CFS)  
Normal flow depth in pipe = 6.75(In.)  
Flow top width inside pipe = 7.79(In.)  
Critical depth could not be calculated.



Pipe flow velocity = 8.92(Ft/s)  
 Travel time through pipe = 0.06 min.  
 Time of concentration (TC) = 12.09 min.

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 105.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 2.350(Ac.)  
 Runoff from this stream = 3.169(CFS)  
 Time of concentration = 12.09 min.  
 Rainfall intensity = 1.827(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 106.000 to Point/Station 107.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 506.000(Ft.)  
 Top (of initial area) elevation = 1557.000(Ft.)  
 Bottom (of initial area) elevation = 1552.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00988 s(percent)= 0.99  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.851 min.  
 Rainfall intensity = 1.845(In/Hr) for a 10.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.737  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 2.121(CFS)  
 Total initial stream area = 1.560(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 107.000 to Point/Station 105.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1552.000(Ft.)  
 Downstream point/station elevation = 1550.500(Ft.)  
 Pipe length = 9.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 2.121(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 2.121(CFS)  
 Normal flow depth in pipe = 4.56(In.)  
 Flow top width inside pipe = 5.13(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 13.25(Ft/s)  
 Travel time through pipe = 0.01 min.  
 Time of concentration (TC) = 11.86 min.

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 105.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 1.560(Ac.)  
 Runoff from this stream = 2.121(CFS)  
 Time of concentration = 11.86 min.  
 Rainfall intensity = 1.844(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	3.169	12.09	1.827
2	2.121	11.86	1.844

Largest stream flow has longer time of concentration  
 $Q_p = 3.169 + \text{sum of } Q_b \cdot \frac{I_a}{I_b} = 2.121 * 0.991 = 2.101$   
 $Q_p = 5.270$   
 Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 3.169 2.121  
 Area of streams before confluence:  
 2.350 1.560  
 Results of confluence:  
 Total flow rate = 5.270(CFS)  
 Time of concentration = 12.090 min.  
 Effective stream area after confluence = 3.910(Ac.)

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 108.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.500(Ft.)  
 Downstream point/station elevation = 1550.000(Ft.)  
 Pipe length = 20.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.270(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 5.270(CFS)  
 Normal flow depth in pipe = 9.21(In.)  
 Flow top width inside pipe = 10.14(In.)  
 Critical Depth = 11.16(In.)  
 Pipe flow velocity = 8.15(Ft/s)  
 Travel time through pipe = 0.04 min.  
 Time of concentration (TC) = 12.13 min.

\*\*\*\*\*  
 Process from Point/Station 108.000 to Point/Station 102.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1550.000(Ft.)  
 End of natural channel elevation = 1549.500(Ft.)  
 Length of natural channel = 80.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 5.345(CFS)  
 Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) = (7 + 8(q(English Units)<sup>0.352</sup>)(slope<sup>0.5</sup>)  
 Velocity using mean channel flow = 1.69(Ft/s)  
 Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0063  
 Corrected/adjusted channel slope = 0.0063  
 Travel time = 0.79 min. TC = 12.92 min.  
 Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.607  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.767(In/Hr) for a 10.0 year storm  
 Subarea runoff = 0.118(CFS) for 0.110(Ac.)  
 Total runoff = 5.388(CFS) Total area = 4.020(Ac.)

\*\*\*\*\*  
 Process from Point/Station 102.000 to Point/Station 102.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 4.020(Ac.)  
 Runoff from this stream = 5.388(CFS)  
 Time of concentration = 12.92 min.  
 Rainfall intensity = 1.767(In/Hr)  
 Summary of stream data:  

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	13.115	13.58	1.724
2	5.388	12.92	1.767

Largest stream flow has longer time of concentration  
 $Q_p = 13.115 + \text{sum of } Q_b \cdot \frac{I_a/I_b}{5.388} = 18.371$   
 $Q_p = 18.371$   
 Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
 13.115      5.388  
 Area of streams before confluence:  
 8.250      4.020  
 Results of confluence:  
 Total flow rate = 18.371(CFS)  
 Time of concentration = 13.578 min.  
 Effective stream area after confluence = 12.270(Ac.)  
 End of computations, total study area = 12.27 (Ac.)  
 The following figures maybe used for a unit hydrograph study of the same area.  
 Area averaged pervious area fraction(Ap) = 0.269  
 Area averaged RI index number = 56.2





Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro100.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District  
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 100.0  
Calculated rainfall intensity data:  
1 hour intensity = 1.200(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 1.000 to Point/Station 1.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Rainfall intensity = 2.078(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.749  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
User specified values are as follows:  
TC = 20.00 min. Rain intensity = 2.08(In/Hr)  
Total area = 0.00(Ac.) Total runoff = 710.00(CFS)

\*\*\*\*\*  
Process from Point/Station 1.000 to Point/Station 2.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1580.500(Ft.)  
Downstream point/station elevation = 1564.000(Ft.)  
Pipe length = 931.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 710.000(CFS)  
Nearest computed pipe diameter = 78.00(In.)  
Calculated individual pipe flow = 710.000(CFS)  
Normal flow depth in pipe = 65.25(In.)  
Flow top width inside pipe = 57.69(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 23.96(Ft/s)  
Travel time through pipe = 0.65 min.  
Time of concentration (TC) = 20.65 min.

\*\*\*\*\*  
Process from Point/Station 2.000 to Point/Station 2.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 0.000(Ac.)  
Runoff from this stream = 710.000(CFS)  
Time of concentration = 20.65 min.  
Rainfall intensity = 2.046(In/Hr)  
Program is now starting with Main Stream No. 2

Process from Point/Station 3.000 to Point/Station 4.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 709.000(Ft.)  
Top (of initial area) elevation = 1584.000(Ft.)  
Bottom (of initial area) elevation = 1573.500(Ft.)  
Difference in elevation = 10.500(Ft.)  
Slope = 0.01481 s(percent)= 1.48  
TC =  $k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 9.622 min.  
Rainfall intensity = 2.997(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.877  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 2.259(CFS)  
Total initial stream area = 0.860(Ac.)  
Pervious area fraction = 0.100

Process from Point/Station 4.000 to Point/Station 5.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1573.500(Ft.)  
Downstream point/station elevation = 1569.000(Ft.)  
Pipe length = 65.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.259(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.259(CFS)  
Normal flow depth in pipe = 4.60(In.)  
Flow top width inside pipe = 9.00(In.)  
Critical Depth = 8.06(In.)  
Pipe flow velocity = 9.94(Ft/s)  
Travel time through pipe = 0.11 min.  
Time of concentration (TC) = 9.73 min.

Process from Point/Station 5.000 to Point/Station 5.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 0.860(Ac.)  
Runoff from this stream = 2.259(CFS)  
Time of concentration = 9.73 min.  
Rainfall intensity = 2.980(In/Hr)

Process from Point/Station 6.000 to Point/Station 7.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 370.000(Ft.)  
Top (of initial area) elevation = 1581.300(Ft.)  
Bottom (of initial area) elevation = 1573.500(Ft.)  
Difference in elevation = 7.800(Ft.)  
Slope = 0.02108 s(percent)= 2.11  
TC =  $k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 6.912 min.  
Rainfall intensity = 3.535(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.879  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 0.808(CFS)  
Total initial stream area = 0.260(Ac.)  
Pervious area fraction = 0.100

Process from Point/Station 7.000 to Point/Station 5.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1573.500(Ft.)  
Downstream point/station elevation = 1469.000(Ft.)  
Pipe length = 44.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.808(CFS)

Nearest computed pipe diameter = 3.00(In.)  
 Calculated individual pipe flow = 0.808(CFS)  
 Normal flow depth in pipe = 1.66(In.)  
 Flow top width inside pipe = 2.98(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 28.92(Ft/s)  
 Travel time through pipe = 0.03 min.  
 Time of concentration (TC) = 6.94 min.

++++++  
 Process from Point/Station 5.000 to Point/Station 5.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 0.260(Ac.)  
 Runoff from this stream = 0.808(CFS)  
 Time of concentration = 6.94 min.  
 Rainfall intensity = 3.529(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.259	9.73	2.980
2	0.808	6.94	3.529

Largest stream flow has longer time of concentration

$Q_p = 2.259 + \text{sum of } Q_b \frac{I_a/I_b}{0.808 * 0.844} = 0.683$   
 $Q_p = 2.942$

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 2.259 0.808  
 Area of streams before confluence:  
 0.860 0.260  
 Results of confluence:  
 Total flow rate = 2.942(CFS)  
 Time of concentration = 9.731 min.  
 Effective stream area after confluence = 1.120(Ac.)

++++++  
 Process from Point/Station 5.000 to Point/Station 8.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1569.000(Ft.)  
 Downstream point/station elevation = 1568.300(Ft.)  
 Pipe length = 139.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 2.942(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 2.942(CFS)  
 Normal flow depth in pipe = 8.74(In.)  
 Flow top width inside pipe = 14.79(In.)  
 Critical Depth = 8.27(In.)  
 Pipe flow velocity = 3.97(Ft/s)  
 Travel time through pipe = 0.58 min.  
 Time of concentration (TC) = 10.32 min.

++++++  
 Process from Point/Station 8.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1568.300(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 166.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 3.270(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $\text{Velocity(ft/s)} = (7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
 velocity using mean channel flow = 0.81(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0018  
 Corrected/adjusted channel slope = 0.0018  
 Travel time = 3.40 min. TC = 13.72 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.672  
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.510(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.422(CFS) for 0.250(Ac.)  
Total runoff = 3.363(CFS) Total area = 1.370(Ac.)

\*\*\*\*\*  
Process from Point/Station 9.000 to Point/Station 9.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.370(Ac.)  
Runoff from this stream = 3.363(CFS)  
Time of concentration = 13.72 min.  
Rainfall intensity = 2.510(In/Hr)

\*\*\*\*\*  
Process from Point/Station 10.000 to Point/Station 11.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 616.000(Ft.)  
Top (of initial area) elevation = 1579.600(Ft.)  
Bottom (of initial area) elevation = 1570.300(Ft.)  
Difference in elevation = 9.300(Ft.)  
Slope = 0.01510 s(percent) = 1.51  
TC =  $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 11.779 min.  
Rainfall intensity = 2.708(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.774  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 4.845(CFS)  
Total initial stream area = 2.310(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 11.000 to Point/Station 12.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1570.300(Ft.)  
Downstream point/station elevation = 1568.300(Ft.)  
Pipe length = 60.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 4.845(CFS)  
Nearest computed pipe diameter = 12.00(In.)  
Calculated individual pipe flow = 4.845(CFS)  
Normal flow depth in pipe = 7.72(In.)  
Flow top width inside pipe = 11.50(In.)  
Critical Depth = 10.90(In.)  
Pipe flow velocity = 9.08(Ft/s)  
Travel time through pipe = 0.11 min.  
Time of concentration (TC) = 11.89 min.

\*\*\*\*\*  
Process from Point/Station 12.000 to Point/Station 9.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1568.300(Ft.)  
End of natural channel elevation = 1568.000(Ft.)  
Length of natural channel = 161.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 4.845(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{0.352})/(\text{slope}^{0.5}))$   
Velocity using mean channel flow = 0.90(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0019  
Corrected/adjusted channel slope = 0.0019  
Travel time = 2.97 min. TC = 14.86 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea



Runoff Coefficient = 0.665  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.411(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 4.845(CFS) Total area = 2.310(Ac.)

++++++  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 2.310(Ac.)  
 Runoff from this stream = 4.845(CFS)  
 Time of concentration = 14.86 min.  
 Rainfall intensity = 2.411(In/Hr)

++++++  
 Process from Point/Station 7.000 to Point/Station 13.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 207.000(Ft.)  
 Top (of initial area) elevation = 1573.500(Ft.)  
 Bottom (of initial area) elevation = 1570.300(Ft.)  
 Difference in elevation = 3.200(Ft.)  
 Slope = 0.01546 s(percent)= 1.55  
 $TC = k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 5.830 min.  
 Rainfall intensity = 3.850(In/Hr) for a 100.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.881  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.712(CFS)  
 Total initial stream area = 0.210(Ac.)  
 Pervious area fraction = 0.100

++++++  
 Process from Point/Station 13.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1570.300(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 161.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 0.712(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{0.5}))$   
 velocity using mean channel flow = 1.69(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0143  
 Corrected/adjusted channel slope = 0.0143  
 Travel time = 1.59 min. TC = 7.42 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.720  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 3.412(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 0.712(CFS) Total area = 0.210(Ac.)

++++++  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
Stream flow area = 0.210(Ac.)  
Runoff from this stream = 0.712(CFS)  
Time of concentration = 7.42 min.  
Rainfall intensity = 3.412(In/Hr)

\*\*\*\*\*  
Process from Point/Station 14.000 to Point/Station 15.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 806.000(Ft.)  
Top (of initial area) elevation = 1581.700(Ft.)  
Bottom (of initial area) elevation = 1569.800(Ft.)  
Difference in elevation = 11.900(Ft.)  
Slope = 0.01476 s(percent)= 1.48  
TC =  $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 13.175 min.  
Rainfall intensity = 2.561(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.769  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 5.753(CFS)  
Total initial stream area = 2.920(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 15.000 to Point/Station 16.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1569.800(Ft.)  
Downstream point/station elevation = 1568.300(Ft.)  
Pipe length = 106.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 5.753(CFS)  
Nearest computed pipe diameter = 15.00(In.)  
Calculated individual pipe flow = 5.753(CFS)  
Normal flow depth in pipe = 9.68(In.)  
Flow top width inside pipe = 14.35(In.)  
Critical Depth = 11.66(In.)  
Pipe flow velocity = 6.87(Ft/s)  
Travel time through pipe = 0.26 min.  
Time of concentration (TC) = 13.43 min.

\*\*\*\*\*  
Process from Point/Station 16.000 to Point/Station 9.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1568.300(Ft.)  
End of natural channel elevation = 1568.000(Ft.)  
Length of natural channel = 148.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 5.753(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{0.352})(\text{slope}^{0.5}))$   
Velocity using mean channel flow = 0.98(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0020  
Corrected/adjusted channel slope = 0.0020  
Travel time = 2.51 min. TC = 15.94 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.659  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.328(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 5.753(CFS) Total area = 2.920(Ac.)

\*\*\*\*\*  
Process from Point/Station 9.000 to Point/Station 9.000

\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 4  
 Stream flow area = 2.920(Ac.)  
 Runoff from this stream = 5.753(CFS)  
 Time of concentration = 15.94 min.  
 Rainfall intensity = 2.328(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 17.000 to Point/Station 18.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 483.000(Ft.)  
 Top (of initial area) elevation = 1575.300(Ft.)  
 Bottom (of initial area) elevation = 1570.500(Ft.)  
 Difference in elevation = 4.800(Ft.)  
 Slope = 0.00994 s(percent)= 0.99  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.619 min.  
 Rainfall intensity = 2.727(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.775  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 4.904(CFS)  
 Total initial stream area = 2.320(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 18.000 to Point/Station 9.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1570.500(Ft.)  
 End of natural channel elevation = 1568.000(Ft.)  
 Length of natural channel = 76.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 4.904(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $Velocity(ft/s) = (7 + 8(q(English\ Units)^{.352})(slope^{0.5}))$   
 Velocity using mean channel flow = 3.81(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0329  
 Corrected/adjusted channel slope = 0.0329  
 Travel time = 0.33 min. TC = 11.95 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.683  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.689(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 4.904(CFS) Total area = 2.320(Ac.)

\*\*\*\*\*  
 Process from Point/Station 9.000 to Point/Station 9.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 5  
 Stream flow area = 2.320(Ac.)  
 Runoff from this stream = 4.904(CFS)  
 Time of concentration = 11.95 min.  
 Rainfall intensity = 2.689(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	3.363	13.72	2.510
2	4.845	14.86	2.411
3	0.712	7.42	3.412

```

4      5.753      15.94      2.328
5      4.904      11.95      2.689
Largest stream flow has longer time of concentration
Qp = 5.753 + sum of
      Qb      Ia/Ib
      3.363 * 0.927 = 3.119
      Qb      Ia/Ib
      4.845 * 0.965 = 4.677
      Qb      Ia/Ib
      0.712 * 0.682 = 0.486
      Qb      Ia/Ib
      4.904 * 0.866 = 4.245
Qp = 18.281

Total of 5 streams to confluence:
Flow rates before confluence point:
      3.363      4.845      0.712      5.753      4.904
Area of streams before confluence:
      1.370      2.310      0.210      2.920      2.320
Results of confluence:
Total flow rate = 18.281(CFS)
Time of concentration = 15.944 min.
Effective stream area after confluence = 9.130(Ac.)

```

```

*****
Process from Point/Station 9.000 to Point/Station 2.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 1568.000(Ft.)
Downstream point/station elevation = 1564.000(Ft.)
Pipe length = 53.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 18.281(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 18.281(CFS)
Normal flow depth in pipe = 10.39(In.)
Flow top width inside pipe = 17.78(In.)
Critical depth could not be calculated.
Pipe flow velocity = 17.28(Ft/s)
Travel time through pipe = 0.05 min.
Time of concentration (TC) = 16.00 min.

```

```

*****
Process from Point/Station 2.000 to Point/Station 2.000
**** CONFLUENCE OF MAIN STREAMS ****

```

```

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 9.130(Ac.)
Runoff from this stream = 18.281(CFS)
Time of concentration = 16.00 min.
Rainfall intensity = 2.324(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	710.000	20.65	2.046
2	18.281	16.00	2.324

Largest stream flow has longer time of concentration

```

Qp = 710.000 + sum of
      Qb      Ia/Ib
      18.281 * 0.880 = 16.090
Qp = 726.090

```

Total of 2 main streams to confluence:

```

Flow rates before confluence point:
      710.000      18.281
Area of streams before confluence:
      0.000      9.130

```

Results of confluence:

```

Total flow rate = 726.090(CFS)
Time of concentration = 20.648 min.
Effective stream area after confluence = 9.130(Ac.)

```

```

*****
Process from Point/Station 2.000 to Point/Station 19.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 1564.000(Ft.)
Downstream point/station elevation = 1553.000(Ft.)
Pipe length = 861.00(Ft.) Manning's N = 0.013

```

No. of pipes = 1 Required pipe flow = 726.090(CFS)  
 Nearest computed pipe diameter = 84.00(In.)  
 Calculated individual pipe flow = 726.090(CFS)  
 Normal flow depth in pipe = 69.28(In.)  
 Flow top width inside pipe = 63.87(In.)  
 Critical Depth = 79.21(In.)  
 Pipe flow velocity = 21.39(Ft/s)  
 Travel time through pipe = 0.67 min.  
 Time of concentration (TC) = 21.32 min.

\*\*\*\*\*  
 Process from Point/Station 19.000 to Point/Station 19.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 1  
 Stream flow area = 9.130(Ac.)  
 Runoff from this stream = 726.090(CFS)  
 Time of concentration = 21.32 min.  
 Rainfall intensity = 2.013(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 18.000 to Point/Station 19.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 662.000(Ft.)  
 Top (of initial area) elevation = 1573.900(Ft.)  
 Bottom (of initial area) elevation = 1567.800(Ft.)  
 Difference in elevation = 6.100(Ft.)  
 Slope = 0.00921 s(percent) = 0.92  
 $TC = k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.294 min.  
 Rainfall intensity = 2.897(In/Hr) for a 100.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.876  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 1.041(CFS)  
 Total initial stream area = 0.410(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station 19.000 to Point/Station 20.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1567.800(Ft.)  
 End of street segment elevation = 1557.500(Ft.)  
 Length of street segment = 589.000(Ft.)  
 Height of curb above gutter flowline = 6.0(In.)  
 Width of half street (curb to crown) = 18.000(Ft.)  
 Distance from crown to crossfall grade break = 16.000(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 2.000(Ft.)  
 Gutter hike from flowline = 2.000(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 1.522(CFS)  
 Depth of flow = 0.265(Ft.), Average velocity = 2.516(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 6.915(Ft.)  
 Flow velocity = 2.52(Ft/s)  
 Travel time = 3.90 min. TC = 14.20 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.873  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Rainfall intensity = 2.467(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.883(CFS) for 0.410(Ac.)  
 Total runoff = 1.924(CFS) Total area = 0.820(Ac.)

Street flow at end of street = 1.924(CFS)  
Half street flow at end of street = 1.924(CFS)  
Depth of flow = 0.282(Ft.); Average velocity = 2.641(Ft/s)  
Flow width (from curb towards crown)= 7.757(Ft.)

\*\*\*\*\*  
Process from Point/Station 20.000 to Point/Station 21.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1556.500(Ft.)  
Pipe length = 71.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.924(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.924(CFS)  
Normal flow depth in pipe = 7.22(In.)  
Flow top width inside pipe = 7.17(In.)  
Critical Depth = 7.59(In.)  
Pipe flow velocity = 5.07(Ft/s)  
Travel time through pipe = 0.23 min.  
Time of concentration (TC) = 14.43 min.

\*\*\*\*\*  
Process from Point/Station 21.000 to Point/Station 23.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1556.500(Ft.)  
End of natural channel elevation = 1556.000(Ft.)  
Length of natural channel = 38.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 2.194(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 2.01(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0132  
Corrected/adjusted channel slope = 0.0132  
Travel time = 0.31 min. TC = 14.74 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.666  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.421(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.371(CFS) for 0.230(Ac.)  
Total runoff = 2.294(CFS) Total area = 1.050(Ac.)

\*\*\*\*\*  
Process from Point/Station 23.000 to Point/Station 23.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.050(Ac.)  
Runoff from this stream = 2.294(CFS)  
Time of concentration = 14.74 min.  
Rainfall intensity = 2.421(In/Hr)

\*\*\*\*\*  
Process from Point/Station 13.000 to Point/Station 22.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 922.000(Ft.)  
Top (of initial area) elevation = 1570.300(Ft.)  
Bottom (of initial area) elevation = 1557.500(Ft.)  
Difference in elevation = 12.800(Ft.)  
Slope = 0.01388 s(percent)= 1.39  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 10.827 min.  
Rainfall intensity = 2.825(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.876  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 1.880(CFS)  
Total initial stream area = 0.760(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 22.000 to Point/Station 21.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1556.500(Ft.)  
Pipe length = 31.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.880(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.880(CFS)  
Normal flow depth in pipe = 5.20(In.)  
Flow top width inside pipe = 8.89(In.)  
Critical Depth = 7.52(In.)  
Pipe flow velocity = 7.12(Ft/s)  
Travel time through pipe = 0.07 min.  
Time of concentration (TC) = 10.90 min.

\*\*\*\*\*  
Process from Point/Station 21.000 to Point/Station 23.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1556.500(Ft.)  
End of natural channel elevation = 1556.000(Ft.)  
Length of natural channel = 38.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 1.880(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.95(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0132  
Corrected/adjusted channel slope = 0.0132  
Travel time = 0.32 min. TC = 11.22 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.688  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.774(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 1.880(CFS) Total area = 0.760(Ac.)

\*\*\*\*\*  
Process from Point/Station 23.000 to Point/Station 23.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 2  
Stream flow area = 0.760(Ac.)  
Runoff from this stream = 1.880(CFS)  
Time of concentration = 11.22 min.  
Rainfall intensity = 2.774(In/Hr)

\*\*\*\*\*  
Process from Point/Station 24.000 to Point/Station 25.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 328.000(Ft.)  
Top (of initial area) elevation = 1570.500(Ft.)  
Bottom (of initial area) elevation = 1566.500(Ft.)  
Difference in elevation = 4.000(Ft.)  
Slope = 0.01220 s(percent) = 1.22  
 $TC = k(0.940)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 23.027 min.  
Rainfall intensity = 1.937(In/Hr) for a 100.0 year storm  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.625  
Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Initial subarea runoff = 0.847(CFS)  
Total initial stream area = 0.700(Ac.)  
Pervious area fraction = 1.000

Process from Point/Station 25.000 to Point/Station 26.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1566.500(Ft.)  
Downstream point/station elevation = 1557.500(Ft.)  
Pipe length = 293.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.847(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 0.847(CFS)  
Normal flow depth in pipe = 4.29(In.)  
Flow top width inside pipe = 5.41(In.)  
Critical Depth = 5.43(In.)  
Pipe flow velocity = 5.63(Ft/s)  
Travel time through pipe = 0.87 min.  
Time of concentration (TC) = 23.89 min.

Process from Point/Station 27.000 to Point/Station 26.000  
\*\*\* SUBAREA FLOW ADDITION \*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.740  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 23.89 min.  
Rainfall intensity = 1.902(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.676(CFS) for 0.480(Ac.)  
Total runoff = 1.523(CFS) Total area = 1.180(Ac.)

Process from Point/Station 26.000 to Point/Station 29.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1557.500(Ft.)  
Downstream point/station elevation = 1557.000(Ft.)  
Pipe length = 39.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 1.523(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 1.523(CFS)  
Normal flow depth in pipe = 6.16(In.)  
Flow top width inside pipe = 8.36(In.)  
Critical Depth = 6.81(In.)  
Pipe flow velocity = 4.72(Ft/s)  
Travel time through pipe = 0.14 min.  
Time of concentration (TC) = 24.03 min.

Process from Point/Station 30.000 to Point/Station 29.000  
\*\*\* SUBAREA FLOW ADDITION \*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.740  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 24.03 min.  
Rainfall intensity = 1.896(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.954(CFS) for 0.680(Ac.)  
Total runoff = 2.477(CFS) Total area = 1.860(Ac.)

Process from Point/Station 29.000 to Point/Station 32.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

Upstream point/station elevation = 1557.000(Ft.)



Downstream point/station elevation = 1556.500(Ft.)  
 Pipe length = 35.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 2.477(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 2.477(CFS)  
 Normal flow depth in pipe = 6.57(In.)  
 Flow top width inside pipe = 11.94(In.)  
 Critical Depth = 8.09(In.)  
 Pipe flow velocity = 5.63(Ft/s)  
 Travel time through pipe = 0.10 min.  
 Time of concentration (TC) = 24.14 min.

\*\*\*\*\*  
 Process from Point/Station 32.000 to Point/Station 23.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1556.500(Ft.)  
 End of natural channel elevation = 1556.000(Ft.)  
 Length of natural channel = 65.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 2.630(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$   
 Velocity using mean channel flow = 1.60(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0077  
 Corrected/adjusted channel slope = 0.0077  
 Travel time = 0.68 min. TC = 24.81 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.618  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 1.866(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.265(CFS) for 0.230(Ac.)  
 Total runoff = 2.742(CFS) Total area = 2.090(Ac.)

\*\*\*\*\*  
 Process from Point/Station 23.000 to Point/Station 23.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
 Stream flow area = 2.090(Ac.)  
 Runoff from this stream = 2.742(CFS)  
 Time of concentration = 24.81 min.  
 Rainfall intensity = 1.866(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	2.294	14.74	2.421
2	1.880	11.22	2.774
3	2.742	24.81	1.866

Largest stream flow has longer time of concentration  
 $Q_p = 2.742 + \text{sum of}$   
 $Q_b \cdot \frac{I_a}{I_b}$   
 $2.294 * 0.771 = 1.769$   
 $Q_b \cdot \frac{I_a}{I_b}$   
 $1.880 * 0.673 = 1.264$   
 $Q_p = 5.775$

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 2.294 1.880 2.742  
 Area of streams before confluence:  
 1.050 0.760 2.090  
 Results of confluence:  
 Total flow rate = 5.775(CFS)  
 Time of concentration = 24.812 min.  
 Effective stream area after confluence = 3.900(Ac.)

\*\*\*\*\*  
 Process from Point/Station 23.000 to Point/Station 19.000

\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1556.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 65.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.775(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 5.775(CFS)  
 Normal flow depth in pipe = 7.78(In.)  
 Flow top width inside pipe = 11.46(In.)  
 Critical Depth = 11.39(In.)  
 Pipe flow velocity = 10.71(Ft/s)  
 Travel time through pipe = 0.10 min.  
 Time of concentration (TC) = 24.91 min.

---

Process from Point/Station 19.000 to Point/Station 19.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 3.900(Ac.)  
 Runoff from this stream = 5.775(CFS)  
 Time of concentration = 24.91 min.  
 Rainfall intensity = 1.862(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	726.090	21.32	2.013
2	5.775	24.91	1.862

Largest stream flow has longer or shorter time of concentration

Qp = 726.090 + sum of  

$$Q_a \quad T_b/T_a$$

$$5.775 * 0.856 = 4.942$$
 Qp = 731.032

Total of 2 main streams to confluence:

Flow rates before confluence point:  
 726.090      5.775  
 Area of streams before confluence:  
 9.130      3.900

Results of confluence:

Total flow rate = 731.032(CFS)  
 Time of concentration = 21.319 min.  
 Effective stream area after confluence = 13.030(Ac.)

---

Process from Point/Station 19.000 to Point/Station 33.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.000(Ft.)  
 Downstream point/station elevation = 1547.000(Ft.)  
 Pipe length = 428.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 731.032(CFS)  
 Nearest computed pipe diameter = 81.00(In.)  
 Calculated individual pipe flow = 731.032(CFS)  
 Normal flow depth in pipe = 72.90(In.)  
 Flow top width inside pipe = 48.60(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 21.57(Ft/s)  
 Travel time through pipe = 0.33 min.  
 Time of concentration (TC) = 21.65 min.

---

Process from Point/Station 33.000 to Point/Station 33.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
 Stream flow area = 13.030(Ac.)  
 Runoff from this stream = 731.032(CFS)  
 Time of concentration = 21.65 min.  
 Rainfall intensity = 1.998(In/Hr)  
 Program is now starting with Main Stream No. 2

---

Process from Point/Station 34.000 to Point/Station 35.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 365.000(Ft.)  
 Top (of initial area) elevation = 1566.000(Ft.)  
 Bottom (of initial area) elevation = 1562.000(Ft.)  
 Difference in elevation = 4.000(Ft.)  
 Slope = 0.01096 s(percent)= 1.10  
 $TC = k(0.940)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 24.552 min.  
 Rainfall intensity = 1.876(In/Hr) for a 100.0 year storm  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.619  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Initial subarea runoff = 1.393(CFS)  
 Total initial stream area = 1.200(Ac.)  
 Pervious area fraction = 1.000

---

\*\*\*\*\*  
 Process from Point/Station 35.000 to Point/Station 36.000  
 \*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

---

Upstream point/station elevation = 1562.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 329.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 1.393(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 1.393(CFS)  
 Normal flow depth in pipe = 4.55(In.)  
 Flow top width inside pipe = 9.00(In.)  
 Critical Depth = 6.52(In.)  
 Pipe flow velocity = 6.22(Ft/s)  
 Travel time through pipe = 0.88 min.  
 Time of concentration (TC) = 25.43 min.

---

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 36.000  
 \*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 1.200(Ac.)  
 Runoff from this stream = 1.393(CFS)  
 Time of concentration = 25.43 min.  
 Rainfall intensity = 1.843(In/Hr)

---

\*\*\*\*\*  
 Process from Point/Station 59.000 to Point/Station 37.000  
 \*\*\* INITIAL AREA EVALUATION \*\*\*

---

Initial area flow distance = 543.000(Ft.)  
 Top (of initial area) elevation = 1564.500(Ft.)  
 Bottom (of initial area) elevation = 1562.000(Ft.)  
 Difference in elevation = 2.500(Ft.)  
 Slope = 0.00460 s(percent)= 0.46  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 14.202 min.  
 Rainfall intensity = 2.466(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.766  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 3.872(CFS)  
 Total initial stream area = 2.050(Ac.)  
 Pervious area fraction = 0.500

---

\*\*\*\*\*  
 Process from Point/Station 37.000 to Point/Station 38.000  
 \*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

---

Upstream point/station elevation = 1562.000(Ft.)  
 Downstream point/station elevation = 1552.000(Ft.)  
 Pipe length = 28.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.872(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 3.872(CFS)  
 Normal flow depth in pipe = 3.91(In.)

Flow top width inside pipe = 8.92(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 21.02(Ft/s)  
 Travel time through pipe = 0.02 min.  
 Time of concentration (TC) = 14.22 min.

\*\*\*\*\*  
 Process from Point/Station 62.000 to Point/Station 38.000  
 \*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.766  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Time of concentration = 14.22 min.  
 Rainfall intensity = 2.465(In/Hr) for a 100.0 year storm  
 Subarea runoff = 3.491(CFS) for 1.850(Ac.)  
 Total runoff = 7.364(CFS) Total area = 3.900(Ac.)

\*\*\*\*\*  
 Process from Point/Station 38.000 to Point/Station 36.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1554.000(Ft.)  
 Downstream point/station elevation = 1553.000(Ft.)  
 Pipe length = 26.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 7.364(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 7.364(CFS)  
 Normal flow depth in pipe = 8.21(In.)  
 Flow top width inside pipe = 14.93(In.)  
 Critical Depth = 12.97(In.)  
 Pipe flow velocity = 10.71(Ft/s)  
 Travel time through pipe = 0.04 min.  
 Time of concentration (TC) = 14.26 min.

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 36.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 3.900(Ac.)  
 Runoff from this stream = 7.364(CFS)  
 Time of concentration = 14.26 min.  
 Rainfall intensity = 2.461(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.393	25.43	1.843
2	7.364	14.26	2.461

Largest stream flow has longer or shorter time of concentration  
 $Q_p = 7.364 + \text{sum of } \frac{Q_a \cdot T_b / T_a}{1.393 * 0.561} = 0.781$   
 $Q_p = 8.145$

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 1.393 7.364  
 Area of streams before confluence:  
 1.200 3.900  
 Results of confluence:  
 Total flow rate = 8.145(CFS)  
 Time of concentration = 14.265 min.  
 Effective stream area after confluence = 5.100(Ac.)

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 40.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.000(Ft.)  
 Downstream point/station elevation = 1552.500(Ft.)  
 Pipe length = 21.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 8.145(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 8.145(CFS)

Normal flow depth in pipe = 10.31(In.)  
Flow top width inside pipe = 13.91(In.)  
Critical Depth = 13.46(In.)  
Pipe flow velocity = 9.06(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 14.30 min.

\*\*\*\*\*  
Process from Point/Station 40.000 to Point/Station 41.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1552.500(Ft.)  
End of natural channel elevation = 1552.000(Ft.)  
Length of natural channel = 80.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 8.377(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.89(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0063  
Corrected/adjusted channel slope = 0.0063  
Travel time = 0.71 min. TC = 15.01 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.664  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.399(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.462(CFS) for 0.290(Ac.)  
Total runoff = 8.607(CFS) Total area = 5.390(Ac.)

\*\*\*\*\*  
Process from Point/Station 41.000 to Point/Station 41.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 5.390(Ac.)  
Runoff from this stream = 8.607(CFS)  
Time of concentration = 15.01 min.  
Rainfall intensity = 2.399(In/Hr)

\*\*\*\*\*  
Process from Point/Station 55.000 to Point/Station 42.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 657.000(Ft.)  
Top (of initial area) elevation = 1561.600(Ft.)  
Bottom (of initial area) elevation = 1553.000(Ft.)  
Difference in elevation = 8.600(Ft.)  
Slope = 0.01309 s(percent) = 1.31  
 $TC = k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 9.567 min.  
Rainfall intensity = 3.005(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.877  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 2.371(CFS)  
Total initial stream area = 0.900(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 42.000 to Point/Station 43.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.000(Ft.)  
Downstream point/station elevation = 1552.500(Ft.)  
Pipe length = 23.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.371(CFS)

Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.371(CFS)  
Normal flow depth in pipe = 7.16(In.)  
Flow top width inside pipe = 7.26(In.)  
Critical Depth = 8.19(In.)  
Pipe flow velocity = 6.29(Ft/s)  
Travel time through pipe = 0.06 min.  
Time of concentration (TC) = 9.63 min.

\*\*\*\*\*  
Process from Point/Station 43.000 to Point/Station 41.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of natural channel elevation = 1552.500(Ft.)  
End of natural channel elevation = 1552.000(Ft.)  
Length of natural channel = 39.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 2.371(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 2.02(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0128  
Corrected/adjusted channel slope = 0.0128  
Travel time = 0.32 min. TC = 9.95 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.698  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.947(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 2.371(CFS) Total area = 0.900(Ac.)

\*\*\*\*\*  
Process from Point/Station 41.000 to Point/Station 41.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 2  
Stream flow area = 0.900(Ac.)  
Runoff from this stream = 2.371(CFS)  
Time of concentration = 9.95 min.  
Rainfall intensity = 2.947(In/Hr)

\*\*\*\*\*  
Process from Point/Station 22.000 to Point/Station 44.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 556.000(Ft.)  
Top (of initial area) elevation = 1557.500(Ft.)  
Bottom (of initial area) elevation = 1553.000(Ft.)  
Difference in elevation = 4.500(Ft.)  
Slope = 0.00809 s(percent) = 0.81  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})^{.2}]$   
Initial area time of concentration = 9.852 min.  
Rainfall intensity = 2.961(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.876  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 1.350(CFS)  
Total initial stream area = 0.520(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 44.000 to Point/Station 45.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.000(Ft.)  
Downstream point/station elevation = 1552.500(Ft.)

Pipe length = 31.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 1.350(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 1.350(CFS)  
 Normal flow depth in pipe = 5.24(In.)  
 Flow top width inside pipe = 8.88(In.)  
 Critical Depth = 6.42(In.)  
 Pipe flow velocity = 5.05(Ft/s)  
 Travel time through pipe = 0.10 min.  
 Time of concentration (TC) = 9.95 min.

\*\*\*\*\*  
 Process from Point/Station 45.000 to Point/Station 41.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1552.500(Ft.)  
 End of natural channel elevation = 1552.000(Ft.)  
 Length of natural channel = 31.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 1.350(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{0.352}) \cdot \text{slope}^{0.5})$   
 velocity using mean channel flow = 2.02(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0161  
 Corrected/adjusted channel slope = 0.0161  
 Travel time = 0.26 min. TC = 10.21 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.696  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.909(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 1.350(CFS) Total area = 0.520(Ac.)

\*\*\*\*\*  
 Process from Point/Station 41.000 to Point/Station 41.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 3  
 Stream flow area = 0.520(Ac.)  
 Runoff from this stream = 1.350(CFS)  
 Time of concentration = 10.21 min.  
 Rainfall intensity = 2.909(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	8.607	15.01	2.399
2	2.371	9.95	2.947
3	1.350	10.21	2.909

Largest stream flow has longer time of concentration

Qp = 8.607 + sum of  
 $Q_b \cdot \frac{I_a}{I_b}$   
 $2.371 * 0.814 = 1.931$   
 $Q_b \cdot \frac{I_a}{I_b}$   
 $1.350 * 0.825 = 1.113$   
 Qp = 11.651

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 8.607 2.371 1.350  
 Area of streams before confluence:  
 5.390 0.900 0.520  
 Results of confluence:  
 Total flow rate = 11.651(CFS)  
 Time of concentration = 15.009 min.  
 Effective stream area after confluence = 6.810(Ac.)

\*\*\*\*\*  
 Process from Point/Station 41.000 to Point/Station 33.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1552.000(Ft.)  
 Downstream point/station elevation = 1547.000(Ft.)  
 Pipe length = 71.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 11.651(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 11.651(CFS)  
 Normal flow depth in pipe = 9.07(In.)  
 Flow top width inside pipe = 14.67(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 15.02(Ft/s)  
 Travel time through pipe = 0.08 min.  
 Time of concentration (TC) = 15.09 min.

++++++  
 Process from Point/Station 33.000 to Point/Station 33.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 6.810(Ac.)  
 Runoff from this stream = 11.651(CFS)  
 Time of concentration = 15.09 min.  
 Rainfall intensity = 2.393(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	731.032	21.65	1.998
2	11.651	15.09	2.393

Largest stream flow has longer time of concentration

$Q_p = 731.032 + \text{sum of } \frac{Q_b \cdot I_a/I_b}{0.835} = 9.726$   
 $Q_p = 740.759$

Total of 2 main streams to confluence:

Flow rates before confluence point:  
 731.032      11.651  
 Area of streams before confluence:  
 13.030      6.810

Results of confluence:

Total flow rate = 740.759(CFS)  
 Time of concentration = 21.649 min.  
 Effective stream area after confluence = 19.840(Ac.)  
 End of computations, total study area = 19.84 (Ac.)  
 The following figures may be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction( $A_p$ ) = 0.486  
 Area averaged RI index number = 56.7



Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro1100.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District  
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 100.0  
Calculated rainfall intensity data:  
1 hour intensity = 1.200(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 58.000 to Point/Station 59.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 933.000(Ft.)  
Top (of initial area) elevation = 1575.900(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)  
Difference in elevation = 11.400(Ft.)  
Slope = 0.01222 s(percent)= 1.22  
TC = k(0.390)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 14.508 min.  
Rainfall intensity = 2.440(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.765  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 4.424(CFS)  
Total initial stream area = 2.370(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 59.000 to Point/Station 60.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
Downstream point/station elevation = 1561.500(Ft.)  
Pipe length = 22.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 4.424(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 4.424(CFS)  
Normal flow depth in pipe = 5.68(In.)  
Flow top width inside pipe = 8.69(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 15.07(Ft/s)  
Travel time through pipe = 0.02 min.  
Time of concentration (TC) = 14.53 min.

\*\*\*\*\*  
Process from Point/Station 60.000 to Point/Station 60.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 2.370(Ac.)

Runoff from this stream = 4.424(CFS)  
 Time of concentration = 14.53 min.  
 Rainfall intensity = 2.438(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 61.000 to Point/Station 62.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 542.000(Ft.)  
 Top (of initial area) elevation = 1572.100(Ft.)  
 Bottom (of initial area) elevation = 1564.500(Ft.)  
 Difference in elevation = 7.600(Ft.)  
 Slope = 0.01402 s(percent)= 1.40  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.358 min.  
 Rainfall intensity = 2.758(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.776  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 2.826(CFS)  
 Total initial stream area = 1.320(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 62.000 to Point/Station 60.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
 Downstream point/station elevation = 1561.500(Ft.)  
 Pipe length = 22.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 2.826(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 2.826(CFS)  
 Normal flow depth in pipe = 4.30(In.)  
 Flow top width inside pipe = 8.99(In.)  
 Critical Depth = 8.54(In.)  
 Pipe flow velocity = 13.56(Ft/s)  
 Travel time through pipe = 0.03 min.  
 Time of concentration (TC) = 11.39 min.

\*\*\*\*\*  
 Process from Point/Station 60.000 to Point/Station 60.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 1.320(Ac.)  
 Runoff from this stream = 2.826(CFS)  
 Time of concentration = 11.39 min.  
 Rainfall intensity = 2.755(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	4.424	14.53	2.438
2	2.826	11.39	2.755

Largest stream flow has longer time of concentration

Qp = 4.424 + sum of  
 $Qb * \frac{Ia}{Ib}$   
 $2.826 * 0.885 = 2.501$   
 Qp = 6.925

Total of 2 streams to confluence:

Flow rates before confluence point:  
 4.424 2.826

Area of streams before confluence:  
 2.370 1.320

Results of confluence:

Total flow rate = 6.925(CFS)  
 Time of concentration = 14.533 min.  
 Effective stream area after confluence = 3.690(Ac.)

\*\*\*\*\*  
 Process from Point/Station 60.000 to Point/Station 63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.500(Ft.)

Downstream point/station elevation = 1561.000(Ft.)  
Pipe length = 33.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 6.925(CFS)  
Nearest computed pipe diameter = 15.00(In.)  
Calculated individual pipe flow = 6.925(CFS)  
Normal flow depth in pipe = 10.83(In.)  
Flow top width inside pipe = 13.44(In.)  
Critical Depth = 12.67(In.)  
Pipe flow velocity = 7.30(Ft/s)  
Travel time through pipe = 0.08 min.  
Time of concentration (TC) = 14.61 min.

\*\*\*\*\*  
Process from Point/Station 63.000 to Point/Station 63.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 3.690(Ac.)  
Runoff from this stream = 6.925(CFS)  
Time of concentration = 14.61 min.  
Rainfall intensity = 2.432(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 64.000 to Point/Station 65.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 888.000(Ft.)  
Top (of initial area) elevation = 1575.100(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)  
Difference in elevation = 10.600(Ft.)  
Slope = 0.01194 s(percent) = 1.19  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 14.291 min.  
Rainfall intensity = 2.459(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.766  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 2.052(CFS)  
Total initial stream area = 1.090(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 65.000 to Point/Station 66.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1564.500(Ft.)  
Downstream point/station elevation = 1561.500(Ft.)  
Pipe length = 25.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.052(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.052(CFS)  
Normal flow depth in pipe = 3.72(In.)  
Flow top width inside pipe = 8.86(In.)  
Critical Depth = 7.78(In.)  
Pipe flow velocity = 11.89(Ft/s)  
Travel time through pipe = 0.04 min.  
Time of concentration (TC) = 14.33 min.

\*\*\*\*\*  
Process from Point/Station 66.000 to Point/Station 66.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.090(Ac.)  
Runoff from this stream = 2.052(CFS)  
Time of concentration = 14.33 min.  
Rainfall intensity = 2.456(In/Hr)

\*\*\*\*\*  
Process from Point/Station 67.000 to Point/Station 68.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 776.000(Ft.)  
Top (of initial area) elevation = 1574.100(Ft.)  
Bottom (of initial area) elevation = 1564.500(Ft.)

Difference in elevation = 9.600(Ft.)  
 Slope = 0.01237 s(percent)= 1.24  
 TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.444 min.  
 Rainfall intensity = 2.535(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.768  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 6.156(CFS)  
 Total initial stream area = 3.160(Ac.)  
 Pervious area fraction = 0.500

++++++  
 Process from Point/Station 68.000 to Point/Station 66.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1564.500(Ft.)  
 Downstream point/station elevation = 1561.500(Ft.)  
 Pipe length = 16.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 6.156(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 6.156(CFS)  
 Normal flow depth in pipe = 6.43(In.)  
 Flow top width inside pipe = 8.13(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 18.23(Ft/s)  
 Travel time through pipe = 0.01 min.  
 Time of concentration (TC) = 13.46 min.

++++++  
 Process from Point/Station 66.000 to Point/Station 66.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 3.160(Ac.)  
 Runoff from this stream = 6.156(CFS)  
 Time of concentration = 13.46 min.  
 Rainfall intensity = 2.534(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.052	14.33	2.456
2	6.156	13.46	2.534

Largest stream flow has longer or shorter time of concentration

$Q_p = 6.156 + \text{sum of}$   
 $Q_a \quad T_b/T_a$   
 $2.052 * 0.939 = 1.928$   
 $Q_p = 8.083$

Total of 2 streams to confluence:

Flow rates before confluence point:

2.052	6.156
-------	-------

Area of streams before confluence:

1.090	3.160
-------	-------

Results of confluence:

Total flow rate = 8.083(CFS)  
 Time of concentration = 13.459 min.  
 Effective stream area after confluence = 4.250(Ac.)

++++++  
 Process from Point/Station 66.000 to Point/Station 63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.500(Ft.)  
 Downstream point/station elevation = 1561.000(Ft.)  
 Pipe length = 25.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 8.083(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 8.083(CFS)  
 Normal flow depth in pipe = 10.97(In.)  
 Flow top width inside pipe = 13.30(In.)  
 Critical Depth = 13.42(In.)  
 Pipe flow velocity = 8.41(Ft/s)  
 Travel time through pipe = 0.05 min.  
 Time of concentration (TC) = 13.51 min.

Process from Point/Station 63.000 to Point/Station 63.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 4.250(Ac.)  
 Runoff from this stream = 8.083(CFS)  
 Time of concentration = 13.51 min.  
 Rainfall intensity = 2.529(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	6.925	14.61	2.432
2	8.083	13.51	2.529

Largest stream flow has longer or shorter time of concentration

Qp = 8.083 + sum of  

$$Q_p = \frac{Q_a}{14.487} * \frac{T_b}{T_a} = \frac{6.925}{14.487} * \frac{0.925}{14.61} = 6.403$$

Total of 2 main streams to confluence:

Flow rates before confluence point:

6.925      8.083

Area of streams before confluence:

3.690      4.250

Results of confluence:

Total flow rate = 14.487(CFS)  
 Time of concentration = 13.508 min.  
 Effective stream area after confluence = 7.940(Ac.)

Process from Point/Station 63.000 to Point/Station 69.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.000(Ft.)  
 Downstream point/station elevation = 1560.500(Ft.)  
 Pipe length = 91.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 14.487(CFS)  
 Nearest computed pipe diameter = 24.00(In.)  
 Calculated individual pipe flow = 14.487(CFS)  
 Normal flow depth in pipe = 17.20(In.)  
 Flow top width inside pipe = 21.63(In.)  
 Critical Depth = 16.44(In.)  
 Pipe flow velocity = 6.01(Ft/s)  
 Travel time through pipe = 0.25 min.  
 Time of concentration (TC) = 13.76 min.

Process from Point/Station 69.000 to Point/Station 57.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1560.500(Ft.)  
 End of natural channel elevation = 1560.000(Ft.)  
 Length of natural channel = 113.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 14.970(CFS)

Natural valley channel type used

L.A. County flood control district formula for channel velocity:

Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{0.352})(\text{slope}^{0.5}))$

Velocity using mean channel flow = 1.85(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)

Normal channel slope = 0.0044

Corrected/adjusted channel slope = 0.0044

Travel time = 1.02 min. TC = 14.78 min.

Adding area flow to channel

UNDEVELOPED (good cover) subarea

Runoff Coefficient = 0.665

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

RI index for soil(AMC 2) = 61.00

Pervious area fraction = 1.000; Impervious fraction = 0.000

Rainfall intensity = 2.418(In/Hr) for a 100.0 year storm

Subarea runoff = 0.853(CFS) for 0.530(Ac.)  
Total runoff = 15.339(CFS) Total area = 8.470(Ac.)

\*\*\*\*\*  
Process from Point/Station 57.000 to Point/Station 57.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 8.470(Ac.)  
Runoff from this stream = 15.339(CFS)  
Time of concentration = 14.78 min.  
Rainfall intensity = 2.418(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 6.000 to Point/Station 54.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 873.000(Ft.)  
Top (of initial area) elevation = 1581.300(Ft.)  
Bottom (of initial area) elevation = 1573.000(Ft.)  
Difference in elevation = 8.300(Ft.)  
Slope = 0.00951 s(percent)= 0.95  
TC =  $k(0.300)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 11.427 min.  
Rainfall intensity = 2.750(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.875  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 3.056(CFS)  
Total initial stream area = 1.270(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 54.000 to Point/Station 55.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1573.000(Ft.)  
End of street segment elevation = 1561.600(Ft.)  
Length of street segment = 542.000(Ft.)  
Height of curb above gutter flowline = 6.0(In.)  
width of half street (curb to crown) = 32.000(Ft.)  
Distance from crown to crossfall grade break = 30.000(Ft.)  
Slope from gutter to grade break (v/hz) = 0.020  
Slope from grade break to crown (v/hz) = 0.020  
Street flow is on [1] side(s) of the street  
Distance from curb to property line = 18.000(Ft.)  
Slope from curb to property line (v/hz) = 0.020  
Gutter width = 2.000(Ft.)  
Gutter hike from flowline = 2.000(In.)  
Manning's N in gutter = 0.0150  
Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 4.525(CFS)  
Depth of flow = 0.345(Ft.), Average velocity = 3.436(Ft/s)  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 10.911(Ft.)  
Flow velocity = 3.44(Ft/s)  
Travel time = 2.63 min. TC = 14.06 min.  
Adding area flow to street  
COMMERCIAL subarea type  
Runoff Coefficient = 0.873  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Rainfall intensity = 2.479(In/Hr) for a 100.0 year storm  
Subarea runoff = 2.858(CFS) for 1.320(Ac.)  
Total runoff = 5.914(CFS) Total area = 2.590(Ac.)  
Street flow at end of street = 5.914(CFS)  
Half street flow at end of street = 5.914(CFS)  
Depth of flow = 0.371(Ft.), Average velocity = 3.658(Ft/s)  
Flow width (from curb towards crown)= 12.208(Ft.)

\*\*\*\*\*

Process from Point/Station 55.000 to Point/Station 56.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1561.600(Ft.)  
 Downstream point/station elevation = 1560.500(Ft.)  
 Pipe length = 159.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.914(CFS)  
 Nearest computed pipe diameter = 18.00(In.)  
 Calculated individual pipe flow = 5.914(CFS)  
 Normal flow depth in pipe = 10.85(In.)  
 Flow top width inside pipe = 17.61(In.)  
 Critical depth = 11.26(In.)  
 Pipe flow velocity = 5.31(Ft/s)  
 Travel time through pipe = 0.50 min.  
 Time of concentration (TC) = 14.55 min.

\*\*\*\*\*  
 Process from Point/Station 56.000 to Point/Station 57.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1560.500(Ft.)  
 End of natural channel elevation = 1560.000(Ft.)  
 Length of natural channel = 90.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 5.914(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 $Velocity(ft/s) = (7 + 8(q(English\ units)^{.352})(slope^{.5}))$   
 Velocity using mean channel flow = 1.64(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0056  
 Corrected/adjusted channel slope = 0.0056  
 Travel time = 0.92 min. TC = 15.47 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.661  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.363(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 5.914(CFS) Total area = 2.590(Ac.)

\*\*\*\*\*  
 Process from Point/Station 57.000 to Point/Station 53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 104.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 5.914(CFS)  
 Nearest computed pipe diameter = 12.00(In.)  
 Calculated individual pipe flow = 5.914(CFS)  
 Normal flow depth in pipe = 7.34(In.)  
 Flow top width inside pipe = 11.70(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 11.76(Ft/s)  
 Travel time through pipe = 0.15 min.  
 Time of concentration (TC) = 15.62 min.

\*\*\*\*\*  
 Process from Point/Station 57.000 to Point/Station 57.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 2.590(Ac.)  
 Runoff from this stream = 5.914(CFS)  
 Time of concentration = 15.62 min.  
 Rainfall intensity = 2.352(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	15.339	14.78	2.418

2            5.914        15.62                    2.352  
 Largest stream flow has longer or shorter time of concentration  
 $Q_p = 15.339 + \text{sum of}$   
 $Q_a \quad T_b/T_a$   
 $5.914 * 0.946 = 5.597$   
 $Q_p = 20.936$

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
     15.339        5.914  
 Area of streams before confluence:  
     8.470        2.590

Results of confluence:  
 Total flow rate = 20.936(CFS)  
 Time of concentration = 14.781 min.  
 Effective stream area after confluence = 11.060(Ac.)

\*\*\*\*\*  
 Process from Point/Station        57.000 to Point/Station        53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 104.00(Ft.)    Manning's N = 0.013  
 No. of pipes = 1    Required pipe flow = 20.936(CFS)  
 Nearest computed pipe diameter = 18.00(In.)  
 Calculated individual pipe flow = 20.936(CFS)  
 Normal flow depth in pipe = 12.52(In.)  
 Flow top width inside pipe = 16.57(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 15.96(Ft/s)  
 Travel time through pipe = 0.11 min.  
 Time of concentration (TC) = 14.89 min.

\*\*\*\*\*  
 Process from Point/Station        53.000 to Point/Station        53.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:  
 In Main Stream number: 1  
 Stream flow area = 11.060(Ac.)  
 Runoff from this stream = 20.936(CFS)  
 Time of concentration = 14.89 min.  
 Rainfall intensity = 2.409(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station        51.000 to Point/Station        52.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 664.000(Ft.)  
 Top (of initial area) elevation = 14574.500(Ft.)  
 Bottom (of initial area) elevation = 1560.000(Ft.)  
 Difference in elevation = 13014.500(Ft.)  
 Slope = 19.60015 s(percent) = 1960.02  
 $TC = k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
 Warning: TC computed to be less than 5 min.; program is assuming the  
 time of concentration is 5 minutes.  
 Initial area time of concentration = 5.000 min.  
 Rainfall intensity = 4.157(In/Hr) for a 100.0 year storm  
 COMMERCIAL subarea type  
 Runoff Coefficient = 0.882  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 8.725(CFS)  
 Total initial stream area = 2.380(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station        52.000 to Point/Station        53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1560.000(Ft.)  
 Downstream point/station elevation = 1554.000(Ft.)  
 Pipe length = 250.00(Ft.)    Manning's N = 0.015  
 No. of pipes = 1    Required pipe flow = 8.725(CFS)  
 Nearest computed pipe diameter = 18.00(In.)



Calculated individual pipe flow = 8.725(CFS)  
 Normal flow depth in pipe = 10.24(In.)  
 Flow top width inside pipe = 17.83(In.)  
 Critical Depth = 13.71(In.)  
 Pipe flow velocity = 8.40(Ft/s)  
 Travel time through pipe = 0.50 min.  
 Time of concentration (TC) = 5.50 min.

\*\*\*\*\*  
 Process from Point/Station 53.000 to Point/Station 53.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Stream flow area = 2.380(Ac.)  
 Runoff from this stream = 8.725(CFS)  
 Time of concentration = 5.50 min.  
 Rainfall intensity = 3.965(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	20.936	14.89	2.409
2	8.725	5.50	3.965

Largest stream flow has longer time of concentration

Qp = 20.936 + sum of  

$$Q_b \frac{I_a/I_b}{8.725 * 0.608} = 5.301$$
  
 Qp = 26.237

Total of 2 main streams to confluence:

Flow rates before confluence point:  
 20.936 8.725  
 Area of streams before confluence:  
 11.060 2.380

Results of confluence:

Total flow rate = 26.237(CFS)  
 Time of concentration = 14.890 min.  
 Effective stream area after confluence = 13.440(Ac.)

\*\*\*\*\*  
 Process from Point/Station 53.000 to Point/Station 70.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1554.000(Ft.)  
 Downstream point/station elevation = 1546.000(Ft.)  
 Pipe length = 416.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 26.237(CFS)  
 Nearest computed pipe diameter = 24.00(In.)  
 Calculated individual pipe flow = 26.237(CFS)  
 Normal flow depth in pipe = 16.78(In.)  
 Flow top width inside pipe = 22.01(In.)  
 Critical Depth = 21.51(In.)  
 Pipe flow velocity = 11.18(Ft/s)  
 Travel time through pipe = 0.62 min.  
 Time of concentration (TC) = 15.51 min.

\*\*\*\*\*  
 Process from Point/Station 70.000 to Point/Station 70.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
 Stream flow area = 13.440(Ac.)  
 Runoff from this stream = 26.237(CFS)  
 Time of concentration = 15.51 min.  
 Rainfall intensity = 2.360(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 71.000 to Point/Station 72.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 424.000(Ft.)  
 Top (of initial area) elevation = 1562.000(Ft.)  
 Bottom (of initial area) elevation = 1553.800(Ft.)  
 Difference in elevation = 8.200(Ft.)  
 Slope = 0.01934 s(percent) = 1.93  
 $TC = k(0.390) * [(length^3)/(elevation change)]^{0.2}$

Initial area time of concentration = 9.654 min.  
Rainfall intensity = 2.992(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.783  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 2.484(CFS)  
Total initial stream area = 1.060(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 72.000 to Point/Station 73.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.800(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 20.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.484(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.484(CFS)  
Normal flow depth in pipe = 3.64(In.)  
Flow top width inside pipe = 8.84(In.)  
Critical Depth = 8.30(In.)  
Pipe flow velocity = 14.81(Ft/s)  
Travel time through pipe = 0.02 min.  
Time of concentration (TC) = 9.68 min.

\*\*\*\*\*  
Process from Point/Station 73.000 to Point/Station 73.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 1.060(Ac.)  
Runoff from this stream = 2.484(CFS)  
Time of concentration = 9.68 min.  
Rainfall intensity = 2.988(In/Hr)

\*\*\*\*\*  
Process from Point/Station 74.000 to Point/Station 75.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 318.000(Ft.)  
Top (of initial area) elevation = 1562.000(Ft.)  
Bottom (of initial area) elevation = 1553.800(Ft.)  
Difference in elevation = 8.200(Ft.)  
Slope = 0.02579 s(percent)= 2.58  
TC =  $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 8.124 min.  
Rainfall intensity = 3.261(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.791  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 4.125(CFS)  
Total initial stream area = 1.600(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 75.000 to Point/Station 73.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1553.800(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 29.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 4.125(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 4.125(CFS)  
Normal flow depth in pipe = 5.49(In.)  
Flow top width inside pipe = 8.78(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 14.62(Ft/s)  
Travel time through pipe = 0.03 min.  
Time of concentration (TC) = 8.16 min.

\*\*\*\*\*  
 Process from Point/Station 73.000 to Point/Station 73.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 1.600(Ac.)  
 Runoff from this stream = 4.125(CFS)  
 Time of concentration = 8.16 min.  
 Rainfall intensity = 3.255(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.484	9.68	2.988
2	4.125	8.16	3.255

Largest stream flow has longer or shorter time of concentration

Qp = 4.125 + sum of  
 Qa Tb/Ta  
 2.484 \* 0.843 = 2.094  
 Qp = 6.219

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 2.484 4.125

Area of streams before confluence:  
 1.060 1.600

Results of confluence:  
 Total flow rate = 6.219(CFS)  
 Time of concentration = 8.157 min.  
 Effective stream area after confluence = 2.660(Ac.)

\*\*\*\*\*  
 Process from Point/Station 73.000 to Point/Station 76.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.000(Ft.)  
 Downstream point/station elevation = 1549.000(Ft.)  
 Pipe length = 152.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 6.219(CFS)  
 Nearest computed pipe diameter = 18.00(In.)  
 Calculated individual pipe flow = 6.219(CFS)  
 Normal flow depth in pipe = 11.41(In.)  
 Flow top width inside pipe = 17.34(In.)  
 Critical Depth = 11.57(In.)  
 Pipe flow velocity = 5.26(Ft/s)  
 Travel time through pipe = 0.48 min.  
 Time of concentration (TC) = 8.64 min.

\*\*\*\*\*  
 Process from Point/Station 76.000 to Point/Station 76.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 2.660(Ac.)  
 Runoff from this stream = 6.219(CFS)  
 Time of concentration = 8.64 min.  
 Rainfall intensity = 3.163(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 52.000 to Point/Station 76.500  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 347.000(Ft.)  
 Top (of initial area) elevation = 1560.000(Ft.)  
 Bottom (of initial area) elevation = 1555.500(Ft.)  
 Difference in elevation = 4.500(Ft.)  
 Slope = 0.01297 s(percent) = 1.30  
 $TC = k(0.390) * [(length^3) / (elevation change)]^{0.2}$   
 Initial area time of concentration = 9.652 min.  
 Rainfall intensity = 2.992(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.783  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 0.937(CFS)  
 Total initial stream area = 0.400(Ac.)  
 Pervious area fraction = 0.500

Process from Point/Station 76.500 to Point/Station 76.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1555.500(Ft.)  
 Downstream point/station elevation = 1549.000(Ft.)  
 Pipe length = 70.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.937(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 0.937(CFS)  
 Normal flow depth in pipe = 3.17(In.)  
 Flow top width inside pipe = 5.99(In.)  
 Critical Depth = 5.59(In.)  
 Pipe flow velocity = 8.91(Ft/s)  
 Travel time through pipe = 0.13 min.  
 Time of concentration (TC) = 9.78 min.

Process from Point/Station 76.000 to Point/Station 76.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 0.400(Ac.)  
 Runoff from this stream = 0.937(CFS)  
 Time of concentration = 9.78 min.  
 Rainfall intensity = 2.972(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	6.219	8.64	3.163
2	0.937	9.78	2.972

Largest stream flow has longer or shorter time of concentration

Qp = 6.219 + sum of  

$$Q_a \frac{T_b}{T_a}$$
 Qp = 0.937 \* 0.883 = 0.828  
 Qp = 7.047

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 6.219 0.937  
 Area of streams before confluence:  
 2.660 0.400  
 Results of confluence:  
 Total flow rate = 7.047(CFS)  
 Time of concentration = 8.638 min.  
 Effective stream area after confluence = 3.060(Ac.)

Process from Point/Station 76.000 to Point/Station 77.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1549.000(Ft.)  
 Downstream point/station elevation = 1548.000(Ft.)  
 Pipe length = 146.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 7.047(CFS)  
 Nearest computed pipe diameter = 18.00(In.)  
 Calculated individual pipe flow = 7.047(CFS)  
 Normal flow depth in pipe = 12.30(In.)  
 Flow top width inside pipe = 16.74(In.)  
 Critical Depth = 12.33(In.)  
 Pipe flow velocity = 5.48(Ft/s)  
 Travel time through pipe = 0.44 min.  
 Time of concentration (TC) = 9.08 min.

Process from Point/Station 77.000 to Point/Station 78.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
 End of natural channel elevation = 1547.500(Ft.)  
 Length of natural channel = 77.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 7.438(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  

$$\text{Velocity(ft/s)} = (7 + 8(q(\text{English Units})^{0.352})(\text{slope}^{0.5}))$$
 velocity using mean channel flow = 1.87(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)

Normal channel slope = 0.0065  
Corrected/adjusted channel slope = 0.0065  
Travel time = 0.69 min. TC = 9.77 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.699  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.974(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.707(CFS) for 0.340(Ac.)  
Total runoff = 7.754(CFS) Total area = 3.400(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 3.400(Ac.)  
Runoff from this stream = 7.754(CFS)  
Time of concentration = 9.77 min.  
Rainfall intensity = 2.974(In/Hr)

\*\*\*\*\*  
Process from Point/Station 79.000 to Point/Station 80.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 227.000(Ft.)  
Top (of initial area) elevation = 1555.200(Ft.)  
Bottom (of initial area) elevation = 1552.500(Ft.)  
Difference in elevation = 2.700(Ft.)  
Slope = 0.01189 s(percent) = 1.19  
TC =  $k(0.390) * [(length^3)/(elevation\ change)]^{0.2}$   
Initial area time of concentration = 8.287 min.  
Rainfall intensity = 3.229(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.790  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 2.040(CFS)  
Total initial stream area = 0.800(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 80.000 to Point/Station 81.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1552.500(Ft.)  
Downstream point/station elevation = 1550.000(Ft.)  
Pipe length = 22.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 2.040(CFS)  
Nearest computed pipe diameter = 9.00(In.)  
Calculated individual pipe flow = 2.040(CFS)  
Normal flow depth in pipe = 3.77(In.)  
Flow top width inside pipe = 8.88(In.)  
Critical Depth = 7.77(In.)  
Pipe flow velocity = 11.64(Ft/s)  
Travel time through pipe = 0.03 min.  
Time of concentration (TC) = 8.32 min.

\*\*\*\*\*  
Process from Point/Station 82.000 to Point/Station 81.000  
\*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

---

SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.790  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Time of concentration = 8.32 min.  
Rainfall intensity = 3.223(In/Hr) for a 100.0 year storm

Subarea runoff = 1.934(CFS) for 0.760(Ac.)  
Total runoff = 3.974(CFS) Total area = 1.560(Ac.)

\*\*\*\*\*  
Process from Point/Station 81.000 to Point/Station 84.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.000(Ft.)  
Downstream point/station elevation = 1548.000(Ft.)  
Pipe length = 230.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 3.974(CFS)  
Nearest computed pipe diameter = 15.00(In.)  
Calculated individual pipe flow = 3.974(CFS)  
Normal flow depth in pipe = 8.89(In.)  
Flow top width inside pipe = 14.74(In.)  
Critical Depth = 9.67(In.)  
Pipe flow velocity = 5.24(Ft/s)  
Travel time through pipe = 0.73 min.  
Time of concentration (TC) = 9.05 min.

\*\*\*\*\*  
Process from Point/Station 84.000 to Point/Station 78.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
End of natural channel elevation = 1547.500(Ft.)  
Length of natural channel = 74.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 3.974(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$   
Velocity using mean channel flow = 1.64(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0068  
Corrected/adjusted channel slope = 0.0068  
Travel time = 0.75 min. TC = 9.80 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.699  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 2.969(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 3.974(CFS) Total area = 1.560(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
Stream flow area = 1.560(Ac.)  
Runoff from this stream = 3.974(CFS)  
Time of concentration = 9.80 min.  
Rainfall intensity = 2.969(In/Hr)

\*\*\*\*\*  
Process from Point/Station 85.000 to Point/Station 86.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 189.000(Ft.)  
Top (of initial area) elevation = 1553.500(Ft.)  
Bottom (of initial area) elevation = 1553.000(Ft.)  
Difference in elevation = 0.500(Ft.)  
Slope =  $0.00265$  s(percent) = 0.26  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 8.002 min.  
Rainfall intensity = 3.286(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.878  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00

Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 0.491(CFS)  
Total initial stream area = 0.170(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 86.000 to Point/Station 87.000  
\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*

---

Upstream point/station elevation = 1553.000(Ft.)  
Downstream point/station elevation = 1548.000(Ft.)  
Pipe length = 34.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 0.491(CFS)  
Nearest computed pipe diameter = 6.00(In.)  
Calculated individual pipe flow = 0.491(CFS)  
Normal flow depth in pipe = 1.95(In.)  
Flow top width inside pipe = 5.62(In.)  
Critical Depth = 4.28(In.)  
Pipe flow velocity = 8.88(Ft/s)  
Travel time through pipe = 0.06 min.  
Time of concentration (TC) = 8.07 min.

\*\*\*\*\*  
Process from Point/Station 87.000 to Point/Station 78.000  
\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*

---

Top of natural channel elevation = 1548.000(Ft.)  
End of natural channel elevation = 1547.500(Ft.)  
Length of natural channel = 23.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 0.491(CFS)

Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) =  $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$   
Velocity using mean channel flow = 1.95(Ft/s)

Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0217  
Corrected/adjusted channel slope = 0.0217  
Travel time = 0.20 min. TC = 8.26 min.

Adding area flow to channel  
UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.712  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Rainfall intensity = 3.234(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
Total runoff = 0.491(CFS) Total area = 0.170(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 78.000  
\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*

---

Along Main Stream number: 2 in normal stream number 3  
Stream flow area = 0.170(Ac.)  
Runoff from this stream = 0.491(CFS)  
Time of concentration = 8.26 min.  
Rainfall intensity = 3.234(In/Hr)

\*\*\*\*\*  
Process from Point/Station 76.500 to Point/Station 88.000  
\*\*\* INITIAL AREA EVALUATION \*\*\*

---

Initial area flow distance = 248.000(Ft.)  
Top (of initial area) elevation = 1555.500(Ft.)  
Bottom (of initial area) elevation = 1553.500(Ft.)  
Difference in elevation = 2.000(Ft.)  
Slope = 0.00806 s(percent) = 0.81  
TC =  $k(0.300)*[(\text{length}^3)/(\text{elevation change})]^{.2}$   
Initial area time of concentration = 7.138 min.  
Rainfall intensity = 3.479(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.879  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.100; Impervious fraction = 0.900  
 Initial subarea runoff = 0.979(CFS)  
 Total initial stream area = 0.320(Ac.)  
 Pervious area fraction = 0.100

\*\*\*\*\*  
 Process from Point/Station 88.000 to Point/Station 89.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1553.500(Ft.)  
 Downstream point/station elevation = 1548.000(Ft.)  
 Pipe length = 37.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 0.979(CFS)  
 Nearest computed pipe diameter = 6.00(In.)  
 Calculated individual pipe flow = 0.979(CFS)  
 Normal flow depth in pipe = 2.83(In.)  
 Flow top width inside pipe = 5.99(In.)  
 Critical Depth = 5.64(In.)  
 Pipe flow velocity = 10.74(Ft/s)  
 Travel time through pipe = 0.06 min.  
 Time of concentration (TC) = 7.20 min.

\*\*\*\*\*  
 Process from Point/Station 89.000 to Point/Station 78.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1548.000(Ft.)  
 End of natural channel elevation = 1547.500(Ft.)  
 Length of natural channel = 5.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 0.979(CFS)

Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) =  $(7 + 8(q(\text{English units})^{.352})(\text{slope}^{.5}))$   
 Velocity using mean channel flow = 4.72(Ft/s)

Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.1000  
 Corrected/adjusted channel slope = 0.1000  
 Travel time = 0.02 min. TC = 7.21 min.

Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.722  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 3.461(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)  
 Total runoff = 0.979(CFS) Total area = 0.320(Ac.)

\*\*\*\*\*  
 Process from Point/Station 78.000 to Point/Station 78.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 4  
 Stream flow area = 0.320(Ac.)  
 Runoff from this stream = 0.979(CFS)  
 Time of concentration = 7.21 min.  
 Rainfall intensity = 3.461(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	7.754	9.77	2.974
2	3.974	9.80	2.969
3	0.491	8.26	3.234
4	0.979	7.21	3.461

Largest stream flow has longer or shorter time of concentration  
 $Q_p = 7.754 + \text{sum of}$   
 $Q_a \cdot \frac{T_b}{T_a}$   
 $3.974 * 0.997 = 3.961$   
 $Q_b \cdot \frac{I_a}{I_b}$   
 $0.491 * 0.920 = 0.451$   
 $Q_b \cdot \frac{I_a}{I_b}$



Qp = 0.979 \* 0.859 = 0.841  
13.008

Total of 4 streams to confluence:  
Flow rates before confluence point:  
7.754 3.974 0.491 0.979  
Area of streams before confluence:  
3.400 1.560 0.170 0.320  
Results of confluence:  
Total flow rate = 13.008(CFS)  
Time of concentration = 9.768 min.  
Effective stream area after confluence = 5.450(Ac.)

\*\*\*\*\*  
Process from Point/Station 78.000 to Point/Station 70.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1547.500(Ft.)  
Downstream point/station elevation = 1546.000(Ft.)  
Pipe length = 79.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 13.008(CFS)  
Nearest computed pipe diameter = 18.00(In.)  
Calculated individual pipe flow = 13.008(CFS)  
Normal flow depth in pipe = 13.34(In.)  
Flow top width inside pipe = 15.77(In.)  
Critical Depth = 16.21(In.)  
Pipe flow velocity = 9.27(Ft/s)  
Travel time through pipe = 0.14 min.  
Time of concentration (TC) = 9.91 min.

\*\*\*\*\*  
Process from Point/Station 70.000 to Point/Station 70.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
Stream flow area = 5.450(Ac.)  
Runoff from this stream = 13.008(CFS)  
Time of concentration = 9.91 min.  
Rainfall intensity = 2.953(In/Hr)  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	26.237	15.51	2.360
2	13.008	9.91	2.953

Largest stream flow has longer time of concentration

Qp = 26.237 + sum of  
Qb Ia/Ib  
13.008 \* 0.799 = 10.398  
Qp = 36.635

Total of 2 main streams to confluence:  
Flow rates before confluence point:  
26.237 13.008  
Area of streams before confluence:  
13.440 5.450

Results of confluence:  
Total flow rate = 36.635(CFS)  
Time of concentration = 15.510 min.  
Effective stream area after confluence = 18.890(Ac.)

\*\*\*\*\*  
Process from Point/Station 70.000 to Point/Station 50.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1546.000(Ft.)  
Downstream point/station elevation = 1545.000(Ft.)  
Pipe length = 25.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 36.635(CFS)  
Nearest computed pipe diameter = 24.00(In.)  
Calculated individual pipe flow = 36.635(CFS)  
Normal flow depth in pipe = 16.38(In.)  
Flow top width inside pipe = 22.34(In.)  
Critical depth could not be calculated.  
Pipe flow velocity = 16.04(Ft/s)  
Travel time through pipe = 0.03 min.  
Time of concentration (TC) = 15.54 min.

\*\*\*\*\*  
 Process from Point/Station 50.000 to Point/Station 50.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 1  
 Stream flow area = 18.890(Ac.)  
 Runoff from this stream = 36.635(CFS)  
 Time of concentration = 15.54 min.  
 Rainfall intensity = 2.358(In/Hr)  
 Program is now starting with Main Stream No. 2

\*\*\*\*\*  
 Process from Point/Station 33.000 to Point/Station 50.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Rainfall intensity = 1.998(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.745  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 User specified values are as follows:  
 TC = 21.65 min. Rain intensity = 2.00(In/Hr)  
 Total area = 19.85(Ac.) Total runoff = 740.76(CFS)

\*\*\*\*\*  
 Process from Point/Station 50.000 to Point/Station 50.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 19.850(Ac.)  
 Runoff from this stream = 740.760(CFS)  
 Time of concentration = 21.65 min.  
 Rainfall intensity = 1.998(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	36.635	15.54	2.358
2	740.760	21.65	1.998

Largest stream flow has longer time of concentration  
 $Q_p = 740.760 + \text{sum of}$   
 $Q_b \quad I_a/I_b$   
 $36.635 * 0.847 = 31.034$   
 $Q_p = 771.794$

Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
 36.635 740.760  
 Area of streams before confluence:  
 18.890 19.850

Results of confluence:  
 Total flow rate = 771.794(CFS)  
 Time of concentration = 21.650 min.  
 Effective stream area after confluence = 38.740(Ac.)  
 End of computations, total study area = 38.74 (Ac.)  
 The following figures may be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.455  
 Area averaged RI index number = 56.1

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0  
Rational Hydrology Study Date: 08/16/21 File:pro2100.out

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

English (in-lb) Units used in input data file

Program License Serial Number 5006

Rational Method Hydrology Program based on  
Riverside County Flood Control & Water Conservation District 1978 hydrology manual  
Storm event (year) = 100.00 Antecedent Moisture Condition = 2  
Standard intensity-duration curves data (Plate D-4.1)  
For the [ Sunnymead-Moreno ] area used.  
10 year storm 10 minute intensity = 2.010(In/Hr)  
10 year storm 60 minute intensity = 0.820(In/Hr)  
100 year storm 10 minute intensity = 2.940(In/Hr)  
100 year storm 60 minute intensity = 1.200(In/Hr)  
Storm event year = 100.0  
Calculated rainfall intensity data:  
1 hour intensity = 1.200(In/Hr)  
Slope of intensity duration curve = 0.5000

\*\*\*\*\*  
Process from Point/Station 51.000 to Point/Station 100.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 462.000(Ft.)  
Top (of initial area) elevation = 1574.500(Ft.)  
Bottom (of initial area) elevation = 1570.800(Ft.)  
Difference in elevation = 3.700(Ft.)  
Slope = 0.00801 s(percent)= 0.80  
TC = k(0.300)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.168 min.  
Rainfall intensity = 3.070(In/Hr) for a 100.0 year storm  
COMMERCIAL subarea type  
Runoff Coefficient = 0.877  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Initial subarea runoff = 3.366(CFS)  
Total initial stream area = 1.250(Ac.)  
Pervious area fraction = 0.100

\*\*\*\*\*  
Process from Point/Station 100.000 to Point/Station 101.000  
\*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1570.800(Ft.)  
End of natural channel elevation = 1559.000(Ft.)  
Length of natural channel = 604.000(Ft.)  
Estimated mean flow rate at midpoint of channel = 12.184(CFS)  
Natural valley channel type used  
L.A. County flood control district formula for channel velocity:  
Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)  
Velocity using mean channel flow = 3.67(Ft/s)  
Correction to map slope used on extremely rugged channels with  
drops and waterfalls (Plate D-6.2)  
Normal channel slope = 0.0195  
Corrected/adjusted channel slope = 0.0195  
Travel time = 2.74 min. TC = 11.91 min.  
Adding area flow to channel  
COMMERCIAL subarea type  
Runoff Coefficient = 0.875  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.100; Impervious fraction = 0.900  
Rainfall intensity = 2.694(In/Hr) for a 100.0 year storm  
Subarea runoff = 15.435(CFS) for 6.550(Ac.)  
Total runoff = 18.800(CFS) Total area = 7.800(Ac.)

\*\*\*\*\*  
Process from Point/Station 101.000 to Point/Station 101.000  
\*\*\*\* SUBAREA FLOW ADDITION \*\*\*\*

---

UNDEVELOPED (good cover) subarea  
Runoff Coefficient = 0.684  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 61.00  
Pervious area fraction = 1.000; Impervious fraction = 0.000  
Time of concentration = 11.91 min.  
Rainfall intensity = 2.694(In/Hr) for a 100.0 year storm  
Subarea runoff = 0.829(CFS) for 0.450(Ac.)  
Total runoff = 19.629(CFS) Total area = 8.250(Ac.)

\*\*\*\*\*  
Process from Point/Station 101.000 to Point/Station 102.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1559.000(Ft.)  
Downstream point/station elevation = 1549.500(Ft.)  
Pipe length = 695.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 19.629(CFS)  
Nearest computed pipe diameter = 24.00(In.)  
Calculated individual pipe flow = 19.629(CFS)  
Normal flow depth in pipe = 15.40(In.)  
Flow top width inside pipe = 23.02(In.)  
Critical Depth = 19.11(In.)  
Pipe flow velocity = 9.22(Ft/s)  
Travel time through pipe = 1.26 min.  
Time of concentration (TC) = 13.16 min.

\*\*\*\*\*  
Process from Point/Station 102.000 to Point/Station 102.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:  
In Main Stream number: 1  
Stream flow area = 8.250(Ac.)  
Runoff from this stream = 19.629(CFS)  
Time of concentration = 13.16 min.  
Rainfall intensity = 2.562(In/Hr)  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 103.000 to Point/Station 104.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

Initial area flow distance = 551.000(Ft.)  
Top (of initial area) elevation = 1558.000(Ft.)  
Bottom (of initial area) elevation = 1552.000(Ft.)  
Difference in elevation = 6.000(Ft.)  
Slope = 0.01089 s(percent)= 1.09  
TC =  $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$   
Initial area time of concentration = 12.026 min.  
Rainfall intensity = 2.680(In/Hr) for a 100.0 year storm  
SINGLE FAMILY (1/4 Acre Lot)  
Runoff Coefficient = 0.774  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
RI index for soil(AMC 2) = 56.00  
Pervious area fraction = 0.500; Impervious fraction = 0.500  
Initial subarea runoff = 4.872(CFS)  
Total initial stream area = 2.350(Ac.)  
Pervious area fraction = 0.500

\*\*\*\*\*  
Process from Point/Station 104.000 to Point/Station 105.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

---

Upstream point/station elevation = 1552.000(Ft.)  
Downstream point/station elevation = 1550.500(Ft.)  
Pipe length = 34.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 4.872(CFS)  
Nearest computed pipe diameter = 12.00(In.)  
Calculated individual pipe flow = 4.872(CFS)  
Normal flow depth in pipe = 7.05(In.)  
Flow top width inside pipe = 11.81(In.)  
Critical Depth = 10.92(In.)

Pipe flow velocity = 10.15(Ft/s)  
 Travel time through pipe = 0.06 min.  
 Time of concentration (TC) = 12.08 min.

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 105.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 2.350(Ac.)  
 Runoff from this stream = 4.872(CFS)  
 Time of concentration = 12.08 min.  
 Rainfall intensity = 2.674(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 106.000 to Point/Station 107.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

Initial area flow distance = 506.000(Ft.)  
 Top (of initial area) elevation = 1557.000(Ft.)  
 Bottom (of initial area) elevation = 1552.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00988 s(percent)= 0.99  
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.851 min.  
 Rainfall intensity = 2.700(In/Hr) for a 100.0 year storm  
 SINGLE FAMILY (1/4 Acre Lot)  
 Runoff Coefficient = 0.774  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 56.00  
 Pervious area fraction = 0.500; Impervious fraction = 0.500  
 Initial subarea runoff = 3.261(CFS)  
 Total initial stream area = 1.560(Ac.)  
 Pervious area fraction = 0.500

\*\*\*\*\*  
 Process from Point/Station 107.000 to Point/Station 105.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1552.000(Ft.)  
 Downstream point/station elevation = 1550.500(Ft.)  
 Pipe length = 9.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 3.261(CFS)  
 Nearest computed pipe diameter = 9.00(In.)  
 Calculated individual pipe flow = 3.261(CFS)  
 Normal flow depth in pipe = 4.41(In.)  
 Flow top width inside pipe = 9.00(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 15.15(Ft/s)  
 Travel time through pipe = 0.01 min.  
 Time of concentration (TC) = 11.86 min.

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 105.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 1.560(Ac.)  
 Runoff from this stream = 3.261(CFS)  
 Time of concentration = 11.86 min.  
 Rainfall intensity = 2.699(In/Hr)  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	4.872	12.08	2.674
2	3.261	11.86	2.699

Largest stream flow has longer time of concentration  
 $Q_p = 4.872 + \text{sum of } Q_b \cdot \frac{I_a}{I_b}$   
 $Q_p = 4.872 + 3.261 * 0.991 = 8.104$   
 Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 4.872 3.261  
 Area of streams before confluence:  
 2.350 1.560  
 Results of confluence:  
 Total flow rate = 8.104(CFS)  
 Time of concentration = 12.082 min.  
 Effective stream area after confluence = 3.910(Ac.)

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 108.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (Program estimated size) \*\*\*\*

Upstream point/station elevation = 1550.500(Ft.)  
 Downstream point/station elevation = 1550.000(Ft.)  
 Pipe length = 20.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 8.104(CFS)  
 Nearest computed pipe diameter = 15.00(In.)  
 Calculated individual pipe flow = 8.104(CFS)  
 Normal flow depth in pipe = 10.09(In.)  
 Flow top width inside pipe = 14.08(In.)  
 Critical Depth = 13.44(In.)  
 Pipe flow velocity = 9.23(Ft/s)  
 Travel time through pipe = 0.04 min.  
 Time of concentration (TC) = 12.12 min.

\*\*\*\*\*  
 Process from Point/Station 108.000 to Point/Station 102.000  
 \*\*\*\* NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of natural channel elevation = 1550.000(Ft.)  
 End of natural channel elevation = 1549.500(Ft.)  
 Length of natural channel = 80.000(Ft.)  
 Estimated mean flow rate at midpoint of channel = 8.218(CFS)  
 Natural valley channel type used  
 L.A. County flood control district formula for channel velocity:  
 Velocity(ft/s) = (7 + 8(q(English Units)<sup>0.352</sup>)(slope<sup>0.5</sup>)  
 Velocity using mean channel flow = 1.88(Ft/s)  
 Correction to map slope used on extremely rugged channels with  
 drops and waterfalls (Plate D-6.2)  
 Normal channel slope = 0.0063  
 Corrected/adjusted channel slope = 0.0063  
 Travel time = 0.71 min. TC = 12.83 min.  
 Adding area flow to channel  
 UNDEVELOPED (good cover) subarea  
 Runoff Coefficient = 0.677  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 RI index for soil(AMC 2) = 61.00  
 Pervious area fraction = 1.000; Impervious fraction = 0.000  
 Rainfall intensity = 2.595(In/Hr) for a 100.0 year storm  
 Subarea runoff = 0.193(CFS) for 0.110(Ac.)  
 Total runoff = 8.297(CFS) Total area = 4.020(Ac.)

\*\*\*\*\*  
 Process from Point/Station 102.000 to Point/Station 102.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

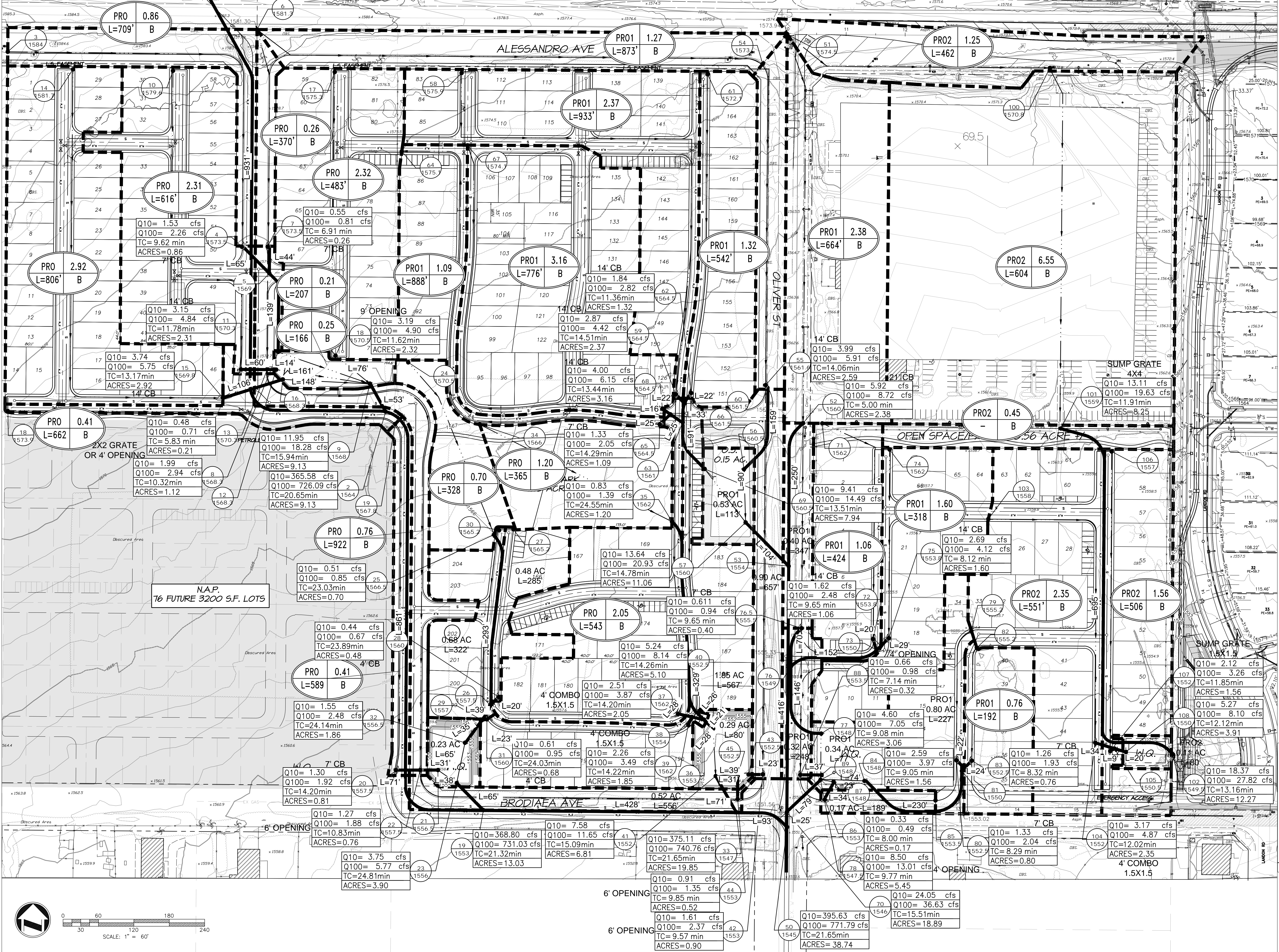
The following data inside Main Stream is listed:  
 In Main Stream number: 2  
 Stream flow area = 4.020(Ac.)  
 Runoff from this stream = 8.297(CFS)  
 Time of concentration = 12.83 min.  
 Rainfall intensity = 2.595(In/Hr)  
 Summary of stream data:  

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	19.629	13.16	2.562
2	8.297	12.83	2.595

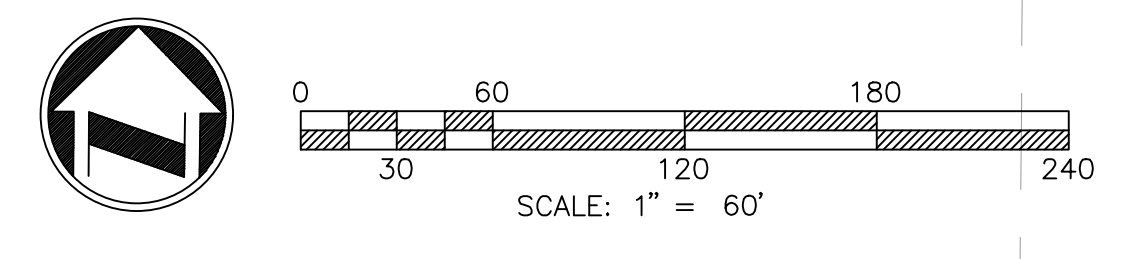
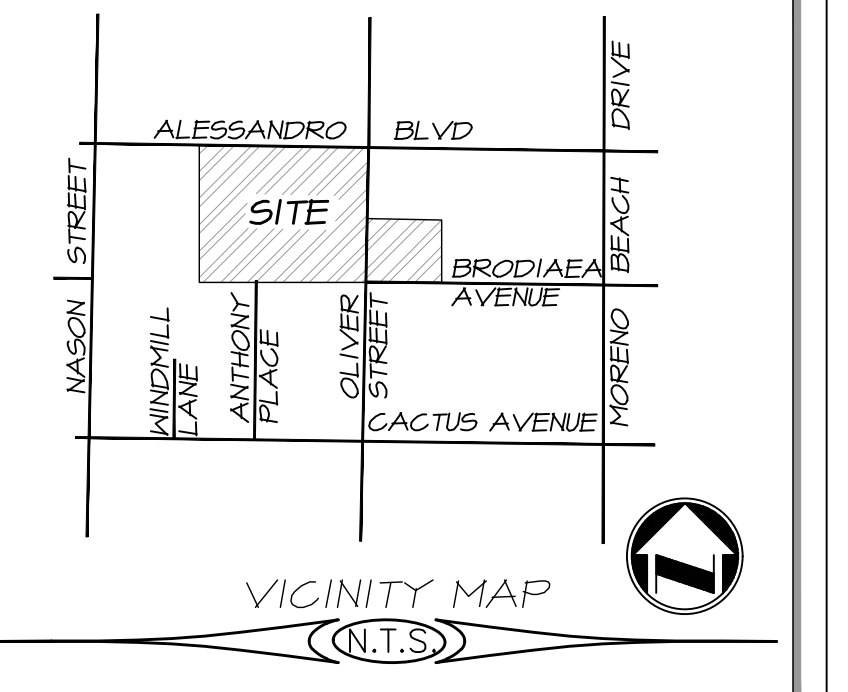
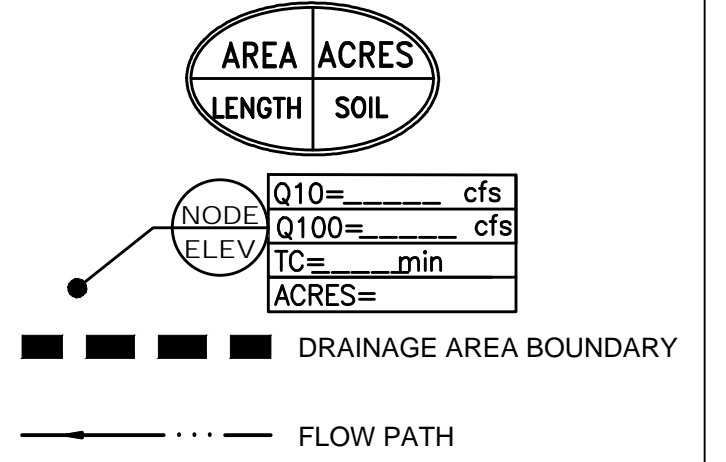
Largest stream flow has longer time of concentration  
 $Q_p = 19.629 + \text{sum of } Q_b \cdot \frac{I_a}{I_b}$   
 $Q_p = 8.297 * 0.987 = 8.190$   
 $Q_p = 27.819$   
 Total of 2 main streams to confluence:  
 Flow rates before confluence point:  
 19.629      8.297  
 Area of streams before confluence:  
 8.250      4.020  
 Results of confluence:  
 Total flow rate = 27.819(CFS)  
 Time of concentration = 13.164 min.  
 Effective stream area after confluence = 12.270(Ac.)  
 End of computations, total study area = 12.27 (Ac.)  
 The following figures maybe used for a unit hydrograph study of the same area.  
 Area averaged pervious area fraction(Ap) = 0.269  
 Area averaged RI index number = 56.2

# POST-DEVELOPMENT RATIONAL HYDROLOGY MAP

TRACT 38236 & 38237



### LEGEND







## **Section 2**

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### **Catch Basin and Street Capacity**



## Node 4 Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 4
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	2.26 cfs
Slope	0.018000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	7.00 ft
Local Depression	8.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	2.26 cfs
Bypass Flow	0.00 cfs
Spread	6.71 ft
Depth	0.25 ft
Flow Area	0.6 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	9.4 in
Velocity	3.96 ft/s
Equivalent Cross Slope	0.321394 ft/ft
Length Factor	1.03
Total Interception Length	6.77 ft

## Node 13

### Worksheet for Curb Inlet on Grade

Project Description	
Worksheet	NODE 13
Type	Grate Inlet On Grade
Solve For	Efficiency
Input Data	
Discharge	0.71 cfs
Slope	0.018000 ft/ft
Gutter Width	2.50 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Grate Width	2.00 ft
Grate Length	2.00 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %
Options	
Grate Flow Option	Exclude None
Results	
Efficiency	1.00
Intercepted Flow	0.71 cfs
Bypass Flow	0.00 cfs
Spread	2.21 ft
Depth	0.18 ft
Flow Area	0.2 ft <sup>2</sup>
Gutter Depression	1.8 in
Total Depression	1.8 in
Velocity	3.62 ft/s
Splash Over Velocity	5.66 ft/s
Frontal Flow Factor	1.00
Side Flow Factor	0.01
Grate Flow Ratio	1.00
Active Grate Length	1.00 ft

# Node 15

## Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 15
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	5.75 cfs
Slope	0.010000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	14.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	5.75 cfs
Bypass Flow	0.00 cfs
Spread	12.03 ft
Depth	0.36 ft
Flow Area	1.6 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	3.67 ft/s
Equivalent Cross Slope	0.170573 ft/ft
Length Factor	1.14
Total Interception Length	12.29 ft

## Node 20

### Worksheet for Curb Inlet on Grade

Project Description	
Worksheet	NODE 20
Type	Curb Inlet On Grade
Solve For	Efficiency
Input Data	
Discharge	1.92 cfs
Slope	0.010000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	7.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft
Results	
Efficiency	1.00
Intercepted Flow	1.92 cfs
Bypass Flow	0.00 cfs
Spread	7.20 ft
Depth	0.26 ft
Flow Area	0.6 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	3.01 ft/s
Equivalent Cross Slope	0.247329 ft/ft
Length Factor	1.13
Total Interception Length	6.21 ft

## Node 28 Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 28
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	0.67 cfs
Slope	0.010000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	4.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	0.67 cfs
Bypass Flow	0.00 cfs
Spread	3.58 ft
Depth	0.19 ft
Flow Area	0.2 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	2.70 ft/s
Equivalent Cross Slope	0.320054 ft/ft
Length Factor	1.17
Total Interception Length	3.42 ft

# Node 31

## Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 31
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	0.95 cfs
Slope	0.010000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	4.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	0.95 cfs
Bypass Flow	0.00 cfs
Spread	4.72 ft
Depth	0.21 ft
Flow Area	0.3 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	2.77 ft/s
Equivalent Cross Slope	0.300311 ft/ft
Length Factor	0.97
Total Interception Length	4.11 ft



## Node 37

### Worksheet for Combination Inlet in Sag

Project Description	
Worksheet	NODE 37
Type	Combination Inlet In Sag
Solve For	Spread
Input Data	
Discharge	3.87 cfs
Local Depression	6.0 in
Local Depression Width	2.00 ft
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	4.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Grate Width	1.50 ft
Grate Length	1.50 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %
Options	
Calculation Option	Use Both
Results	
Spread	1.73 ft
Throat Incline Angle	90.00 degrees
Depth	0.07 ft
Gutter Depression	2.9 in
Total Depression	8.9 in
Open Grate Area	1.0 ft <sup>2</sup>
Active Grate Weir Length	3.00 ft

## Node 39

### Worksheet for Combination Inlet in Sag

Project Description	
Worksheet	NODE 39
Type	Combination Inlet In Sag
Solve For	Spread
Input Data	
Discharge	3.49 cfs
Local Depression	6.0 in
Local Depression Width	2.00 ft
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	4.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Grate Width	1.50 ft
Grate Length	1.50 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %
Options	
Calculation Option	Use Both
Results	
Spread	1.61 ft
Throat Incline Angle	90.00 degrees
Depth	0.03 ft
Gutter Depression	2.9 in
Total Depression	8.9 in
Open Grate Area	1.0 ft <sup>2</sup>
Active Grate Weir Length	3.00 ft

## Node 42 Worksheet for Curb Cutout

---

Project Description	
Worksheet	NODE 42
Flow Element	Rectangular Channel
Method	Manning's Formula
Solve For	Channel Depth

---

Input Data	
Mannings Coefficient	0.013
Slope	0.001000 ft/ft
Bottom Width	6.00 ft
Discharge	2.37 cfs

---

Results	
Depth	0.27 ft
Flow Area	1.6 ft <sup>2</sup>
Wetted Perimeter	6.55 ft
Top Width	6.00 ft
Critical Depth	0.17 ft
Critical Slope	0.004790 ft/ft
Velocity	1.44 ft/s
Velocity Head	0.03 ft
Specific Energy	0.31 ft
Froude Number	0.48
Flow Type	Subcritical

## Node 55

### Worksheet for Curb Inlet on Grade

Project Description	
Worksheet	NODE 55
Type	Curb Inlet On Grade
Solve For	Efficiency
Input Data	
Discharge	5.91 cfs
Slope	0.016000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	14.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft
Results	
Efficiency	1.00
Intercepted Flow	5.91 cfs
Bypass Flow	0.00 cfs
Spread	10.99 ft
Depth	0.34 ft
Flow Area	1.3 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	4.45 ft/s
Equivalent Cross Slope	0.183401 ft/ft
Length Factor	1.02
Total Interception Length	13.71 ft

## Node 59

### Worksheet for Curb Inlet on Grade

Project Description	
Worksheet	NODE 59
Type	Curb Inlet On Grade
Solve For	Efficiency
Input Data	
Discharge	4.42 cfs
Slope	0.016000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	14.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft
Results	
Efficiency	1.00
Intercepted Flow	4.42 cfs
Bypass Flow	0.00 cfs
Spread	9.65 ft
Depth	0.31 ft
Flow Area	1.1 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	4.21 ft/s
Equivalent Cross Slope	0.202811 ft/ft
Length Factor	1.23
Total Interception Length	11.42 ft

## Node 62

### Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 62
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	2.82 cfs
Slope	0.016000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	14.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	2.82 cfs
Bypass Flow	0.00 cfs
Spread	7.77 ft
Depth	0.28 ft
Flow Area	0.7 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	3.89 ft/s
Equivalent Cross Slope	0.235791 ft/ft
Length Factor	1.62
Total Interception Length	8.64 ft

# Node 65

## Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 65
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	2.05 cfs
Slope	0.013000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	7.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	2.05 cfs
Bypass Flow	0.00 cfs
Spread	6.95 ft
Depth	0.26 ft
Flow Area	0.6 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	3.40 ft/s
Equivalent Cross Slope	0.252447 ft/ft
Length Factor	1.03
Total Interception Length	6.82 ft

# Node 75

## Worksheet for Curb Inlet in Sag

---

Project Description	
Worksheet	NODE 75
Type	Curb Inlet In Sag
Solve For	Spread

---

Input Data	
Discharge	4.12 cfs
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	14.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Spread	9.63 ft
Throat Incline Angle	90.00 degrees
Depth	0.43 ft
Gutter Depression	2.9 in
Total Depression	8.9 in



## Node 76.5

### Worksheet for Curb Inlet on Grade

---

Project Description	
Worksheet	NODE 76.5
Type	Curb Inlet On Grade
Solve For	Efficiency

---

Input Data	
Discharge	0.94 cfs
Slope	0.016000 ft/ft
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Mannings Coefficient	0.013
Curb Opening Length	7.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Efficiency	1.00
Intercepted Flow	0.94 cfs
Bypass Flow	0.00 cfs
Spread	3.92 ft
Depth	0.20 ft
Flow Area	0.3 ft <sup>2</sup>
Gutter Depression	1.4 in
Total Depression	7.4 in
Velocity	3.44 ft/s
Equivalent Cross Slope	0.315078 ft/ft
Length Factor	1.53
Total Interception Length	4.58 ft

# Node 80

## Worksheet for Curb Inlet in Sag

---

### Project Description

---

Worksheet	NODE 80
Type	Curb Inlet In Sag
Solve For	Spread

---

### Input Data

---

Discharge	2.04 cfs
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	7.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

### Results

---

Spread	7.87 ft
Throat Incline Angle	90.00 degrees
Depth	0.40 ft
Gutter Depression	2.9 in
Total Depression	8.9 in

# Node 83

## Worksheet for Curb Inlet in Sag

---

Project Description	
Worksheet	NODE 83
Type	Curb Inlet In Sag
Solve For	Spread

---

Input Data	
Discharge	1.93 cfs
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	7.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Local Depression	6.0 in
Local Depression Width	2.00 ft

---

Results	
Spread	7.59 ft
Throat Incline Angle	90.00 degrees
Depth	0.39 ft
Gutter Depression	2.9 in
Total Depression	8.9 in

# Node 86

## Worksheet for Curb Cutout

---

Project Description	
Worksheet	NODE 86
Flow Element	Rectangular Channel
Method	Manning's Formula
Solve For	Channel Depth

---

Input Data	
Mannings Coefficient	0.013
Slope	0.001000 ft/ft
Bottom Width	4.00 ft
Discharge	0.49 cfs

---

Results	
Depth	0.13 ft
Flow Area	0.5 ft <sup>2</sup>
Wetted Perimeter	4.27 ft
Top Width	4.00 ft
Critical Depth	0.08 ft
Critical Slope	0.006075 ft/ft
Velocity	0.91 ft/s
Velocity Head	0.01 ft
Specific Energy	0.15 ft
Froude Number	0.44
Flow Type	Subcritical

# Node 88

## Worksheet for Curb Cutout

---

Project Description	
Worksheet	NODE 88
Flow Element	Rectangular Channel
Method	Manning's Formula
Solve For	Channel Depth

---

Input Data	
Mannings Coefficient	0.013
Slope	0.001000 ft/ft
Bottom Width	4.00 ft
Discharge	0.98 cfs

---

Results	
Depth	0.21 ft
Flow Area	0.8 ft <sup>2</sup>
Wetted Perimeter	4.41 ft
Top Width	4.00 ft
Critical Depth	0.12 ft
Critical Slope	0.005361 ft/ft
Velocity	1.18 ft/s
Velocity Head	0.02 ft
Specific Energy	0.23 ft
Froude Number	0.46
Flow Type	Subcritical

# Node 101

## Worksheet for Grate Inlet In Sag

---

Project Description	
Worksheet	NODE 101
Type	Grate Inlet In Sag
Solve For	Spread

---

Input Data	
Discharge	19.63 cfs
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Grate Width	4.00 ft
Grate Length	4.00 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %

---

Results	
Spread	6.73 ft
Depth	0.37 ft
Gutter Depression	2.9 in
Total Depression	8.9 in
Open Grate Area	7.2 ft <sup>2</sup>
Active Grate Weir Length	8.00 ft

# Node 104

## Worksheet for Combination Inlet in Sag

---

Project Description	
Worksheet	NODE 104
Type	Combination Inlet In Sag
Solve For	Spread

---

---

Input Data	
Discharge	4.87 cfs
Local Depression	6.0 in
Local Depression Width	2.00 ft
Gutter Width	4.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Curb Opening Length	4.00 ft
Opening Height	0.67 ft
Curb Throat Type	Horizontal
Grate Width	1.50 ft
Grate Length	1.50 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %

---

---

Options	
Calculation Option	Use Both

---

---

Results	
Spread	3.32 ft
Throat Incline Angle	90.00 degrees
Depth	0.27 ft
Gutter Depression	2.9 in
Total Depression	8.9 in
Open Grate Area	1.0 ft <sup>2</sup>
Active Grate Weir Length	3.00 ft

# Node 107

## Worksheet for Grate inlet in Sag

---

Project Description	
Worksheet	NODE 107
Type	Grate Inlet In Sag
Solve For	Spread

---

Input Data	
Discharge	3.26 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.080000 ft/ft
Road Cross Slope	0.020000 ft/ft
Grate Width	1.50 ft
Grate Length	1.50 ft
Local Depression	6.0 in
Local Depression Width	2.00 ft
Grate Type	P-50 mm (P-1-7/8")
Clogging	50.0 %

---

Results	
Spread	1.54 ft
Depth	0.01 ft
Gutter Depression	1.4 in
Total Depression	7.4 in
Open Grate Area	1.0 ft <sup>2</sup>
Active Grate Weir Length	3.00 ft



# Private Streets Worksheet for Irregular Channel

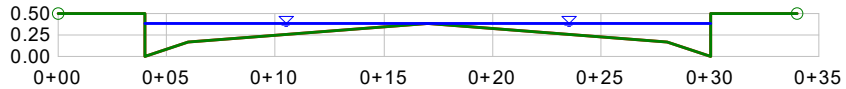
Project Description	
Worksheet	Private Streets
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data	
Slope	0.010000 ft/ft
Water Surface Elevation	0.38 ft

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Elevation Range	0.00 to 0.50
Discharge	9.45 cfs
Flow Area	3.6 ft <sup>2</sup>
Wetted Perimeter	26.78 ft
Top Width	26.00 ft
Actual Depth	0.38 ft
Critical Elevation	0.40 ft
Critical Slope	0.006293 ft/ft
Velocity	2.61 ft/s
Velocity Head	0.11 ft
Specific Energy	0.49 ft
Froude Number	1.23
Flow Type	Supercritical

Calculation Messages:  
Flow is divided.

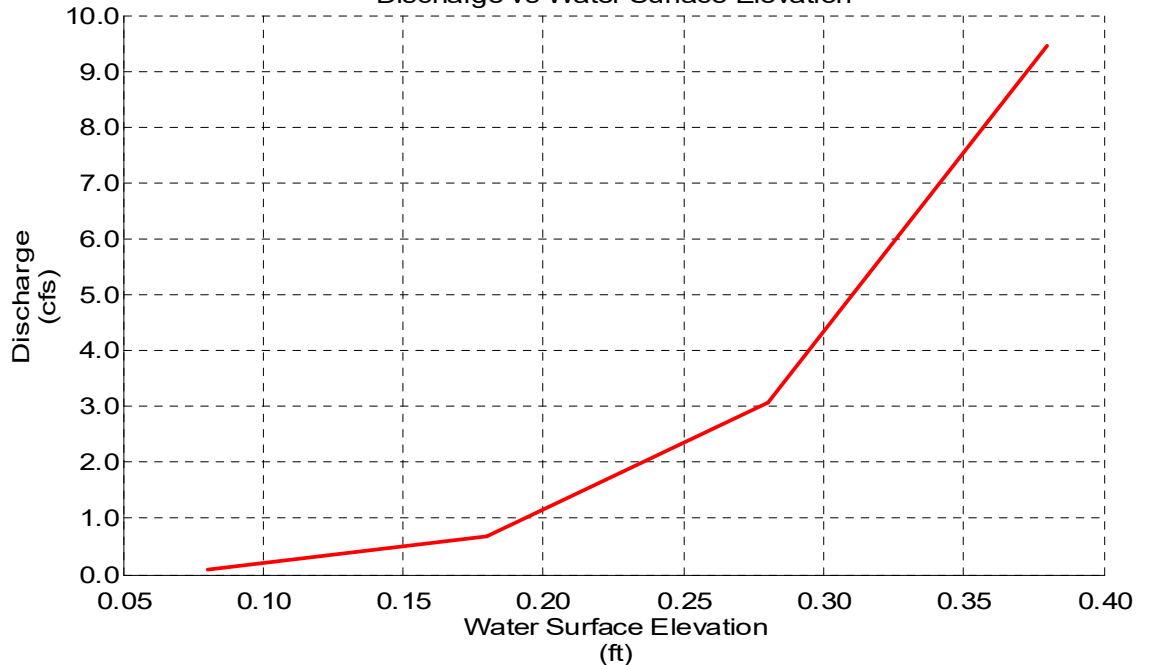


Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00	0+34	0.015

V:4.0  
H:1  
NTS

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00	0.50
0+04	0.50
0+04	0.00
0+06	0.16
0+17	0.38
0+28	0.16
0+30	0.00
0+30	0.50
0+34	0.50

Worksheet: Private Streets  
Discharge vs Water Surface Elevation



# Street B & C

## Worksheet for Irregular Channel

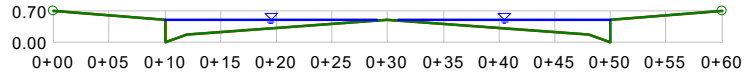
Project Description	
Worksheet	Street B & C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data	
Slope	0.010000 ft/ft
Water Surface Elevation	0.50 ft

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Elevation Range	0.00 to 0.70
Discharge	24.53 cfs
Flow Area	7.5 ft <sup>2</sup>
Wetted Perimeter	39.02 ft
Top Width	38.00 ft
Actual Depth	0.50 ft
Critical Elevation	0.55 ft
Critical Slope	0.005677 ft/ft
Velocity	3.29 ft/s
Velocity Head	0.17 ft
Specific Energy	0.67 ft
Froude Number	1.31
Flow Type	Supercritical

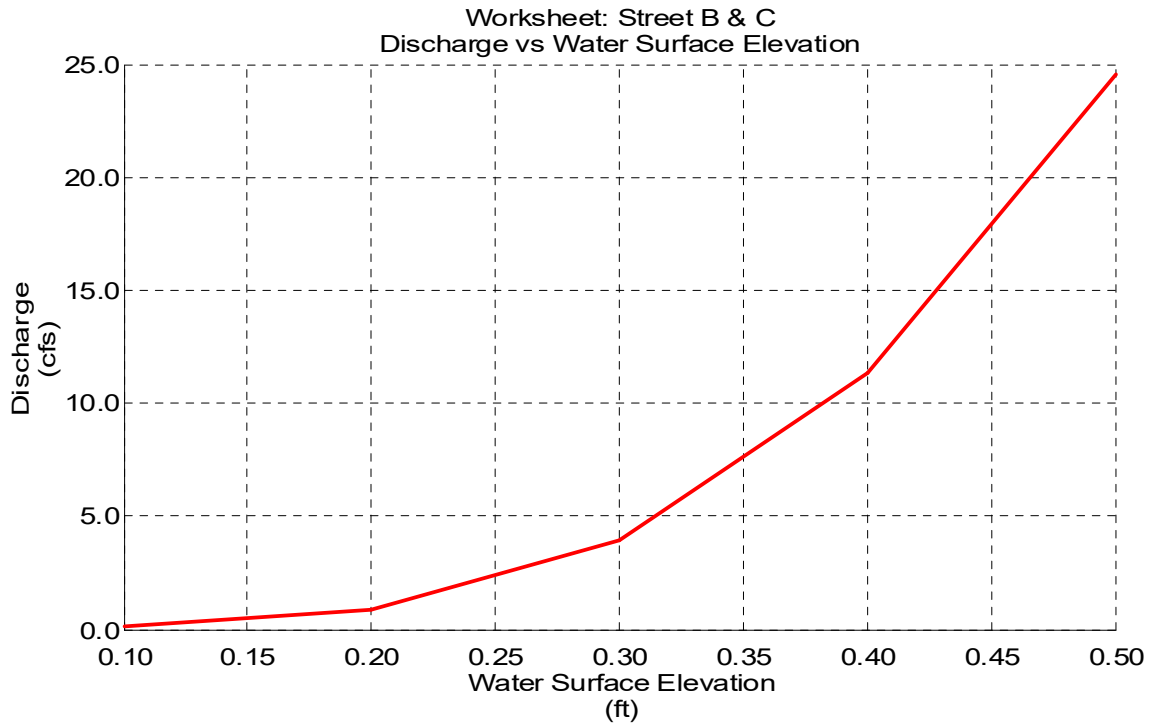
Calculation Messages:  
Flow is divided.



Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00	0+60	0.015

V:4.0  
H:1  
NTS

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00	0.70
0+10	0.50
0+10	0.00
0+12	0.16
0+30	0.52
0+48	0.16
0+50	0.00
0+50	0.50
0+60	0.70

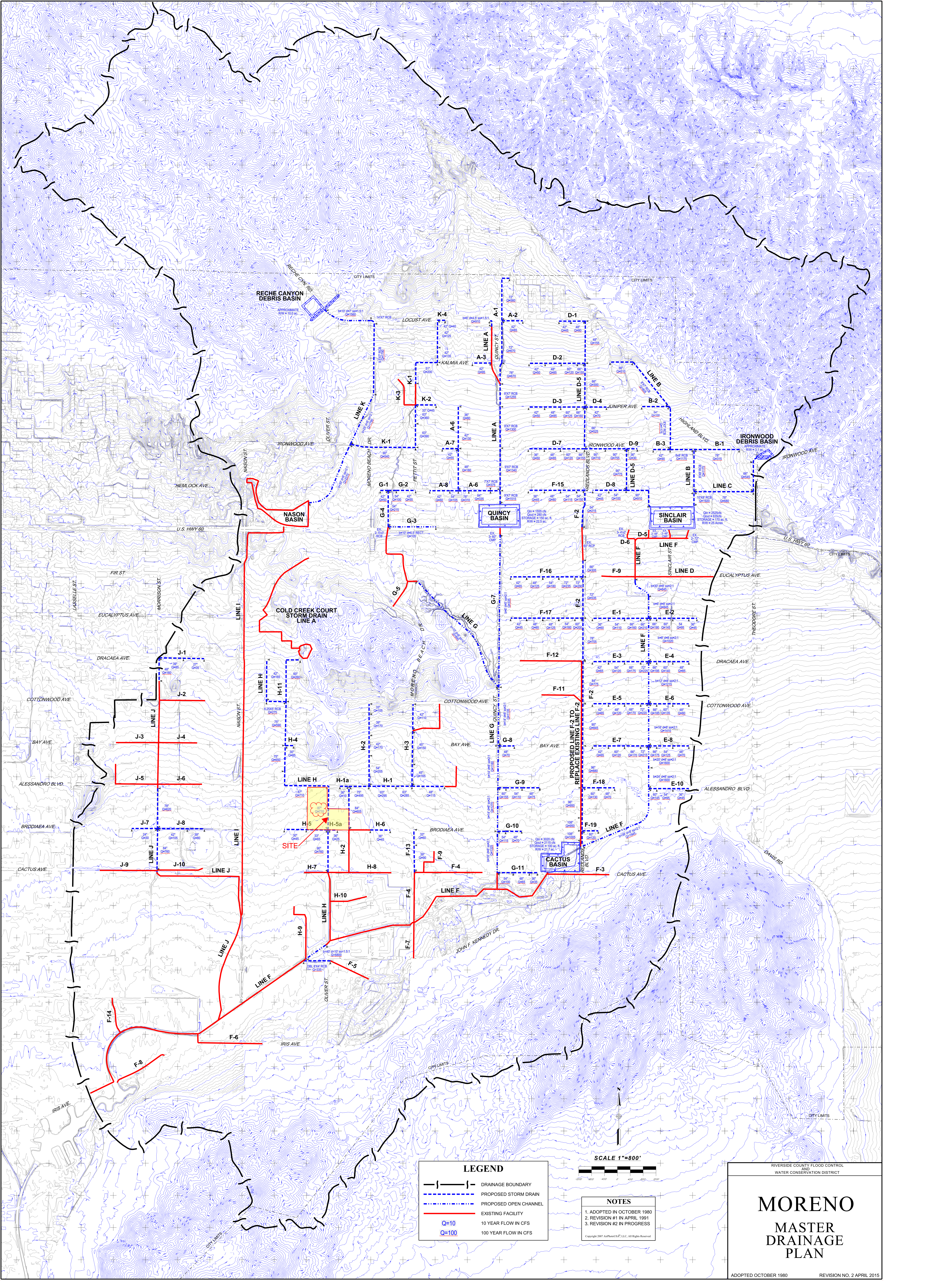


## **Section 3**

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### **Approved Offsite Hydrology Maps and MDP Storm Drain Plans**





**LEGEND**

	DRAINAGE BOUNDARY
	PROPOSED STORM DRAIN
	PROPOSED OPEN CHANNEL
	EXISTING FACILITY
	10 YEAR FLOW IN CFS
	100 YEAR FLOW IN CFS



**NOTES**

1. ADOPTED IN OCTOBER 1980
2. REVISION #1 IN APRIL 1991
3. REVISION #2 IN PROGRESS

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RIVERSIDE COUNTY FLOOD CONTROL  
WATER CONSERVATION DISTRICT

# MORENO

## MASTER DRAINAGE PLAN

ADOPTED OCTOBER 1980      REVISION NO. 2 APRIL 2015



## **Section 4**

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### **Riverside County Plates**





RUNOFF INDEX NUMBERS OF HYDROLOGIC SOIL-COVER COMPLEXES FOR PERVIOUS AREAS-AMC II

Cover Type (3)	Quality of Cover (2)	Soil Group			
		A	B	C	D
<b><u>NATURAL COVERS -</u></b>					
Barren (Rockland, eroded and graded land)		78	86	91	93
Chaparrel, Broadleaf (Manzonita, ceanothus and scrub oak)	Poor	53	70	80	85
	Fair	40	63	75	81
	Good	31	57	71	78
Chaparrel, Narrowleaf (Chamise and redshank)	Poor	71	82	88	91
	Fair	55	72	81	86
Grass, Annual or Perennial	Poor	67	78	86	89
	Fair	50	69	79	84
	Good	38	61	74	80
Meadows or Cienegas (Areas with seasonally high water table, principal vegetation is sod forming grass)	Poor	63	77	85	88
	Fair	51	70	80	84
	Good	30	58	72	78
Open Brush (Soft wood shrubs - buckwheat, sage, etc.)	Poor	62	76	84	88
	Fair	46	66	77	83
	Good	41	63	75	81
Woodland (Coniferous or broadleaf trees predominate. Canopy density is at least 50 percent)	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	28	55	70	77
Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)	Poor	57	73	82	86
	Fair	44	65	77	82
	Good	33	58	72	79
<b><u>URBAN COVERS -</u></b>					
Residential or Commercial Landscaping (Lawn, shrubs, etc.)	Good	32	56	69	75
Turf (Irrigated and mowed grass)	Poor	58	74	83	87
	Fair	44	65	77	82
	Good	33	58	72	79
<b><u>AGRICULTURAL COVERS -</u></b>					
Fallow (Land plowed but not tilled or seeded)		76	85	90	92

**RCFC & WCD**  
HYDROLOGY MANUAL

RUNOFF INDEX NUMBERS  
FOR  
PERVIOUS AREA

ACTUAL IMPERVIOUS COVER

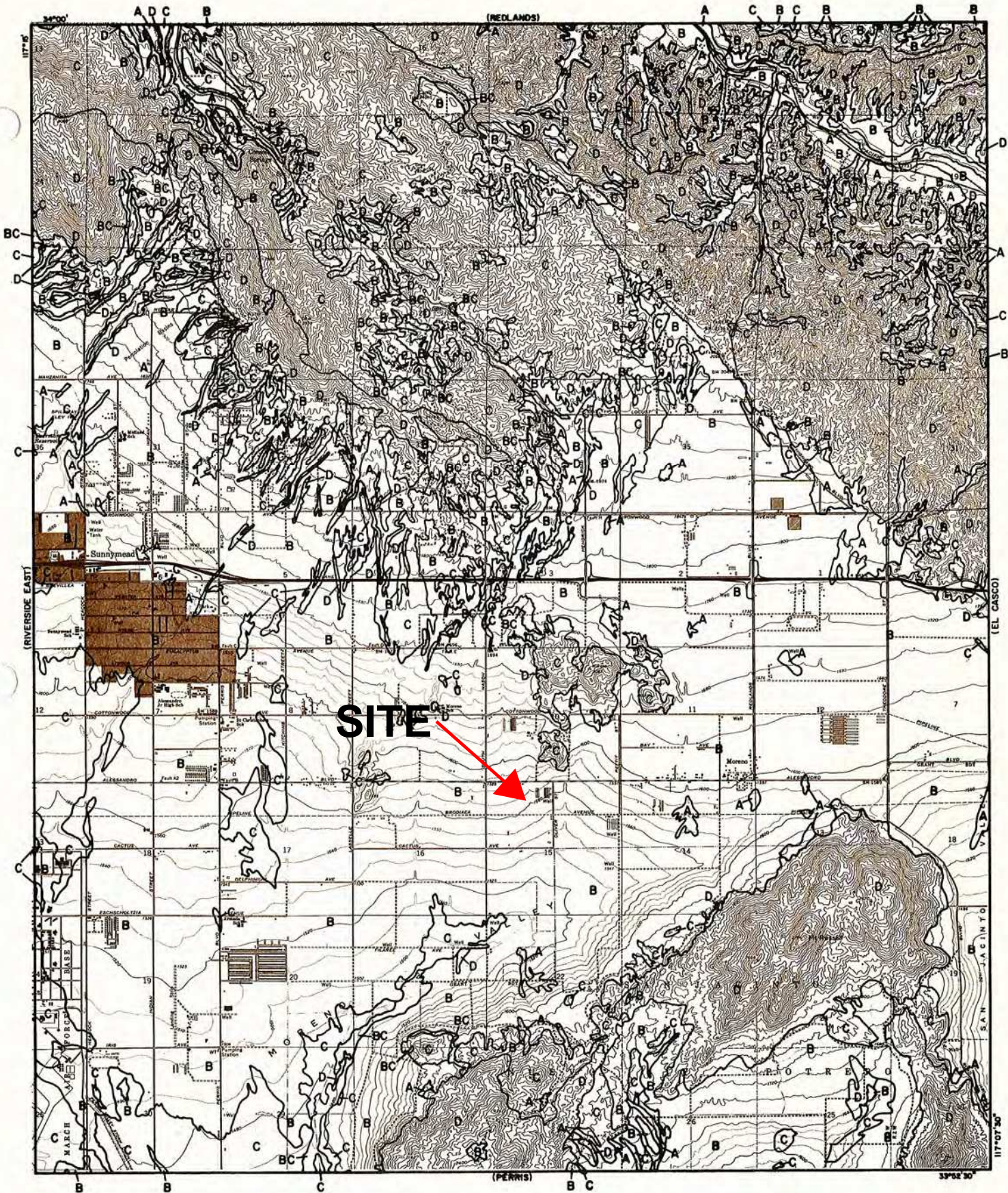
Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent (2)
Natural or Agriculture	0 - 10	0
Single Family Residential: (3)		
40,000 S. F. (1 Acre) Lots	10 - 25	20
20,000 S. F. (½ Acre) Lots	30 - 45	40
7,200 - 10,000 S. F. Lots	45 - 55	50
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 -100	90

Notes:

1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.
2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area should always be made, and a review of aerial photos, where available may assist in estimating the percentage of impervious cover in developed areas.
3. For typical horse ranch subdivisions increase impervious area 5 percent over the values recommended in the table above.

**RCFC & WCD**  
HYDROLOGY MANUAL

**IMPERVIOUS COVER  
FOR  
DEVELOPED AREAS**



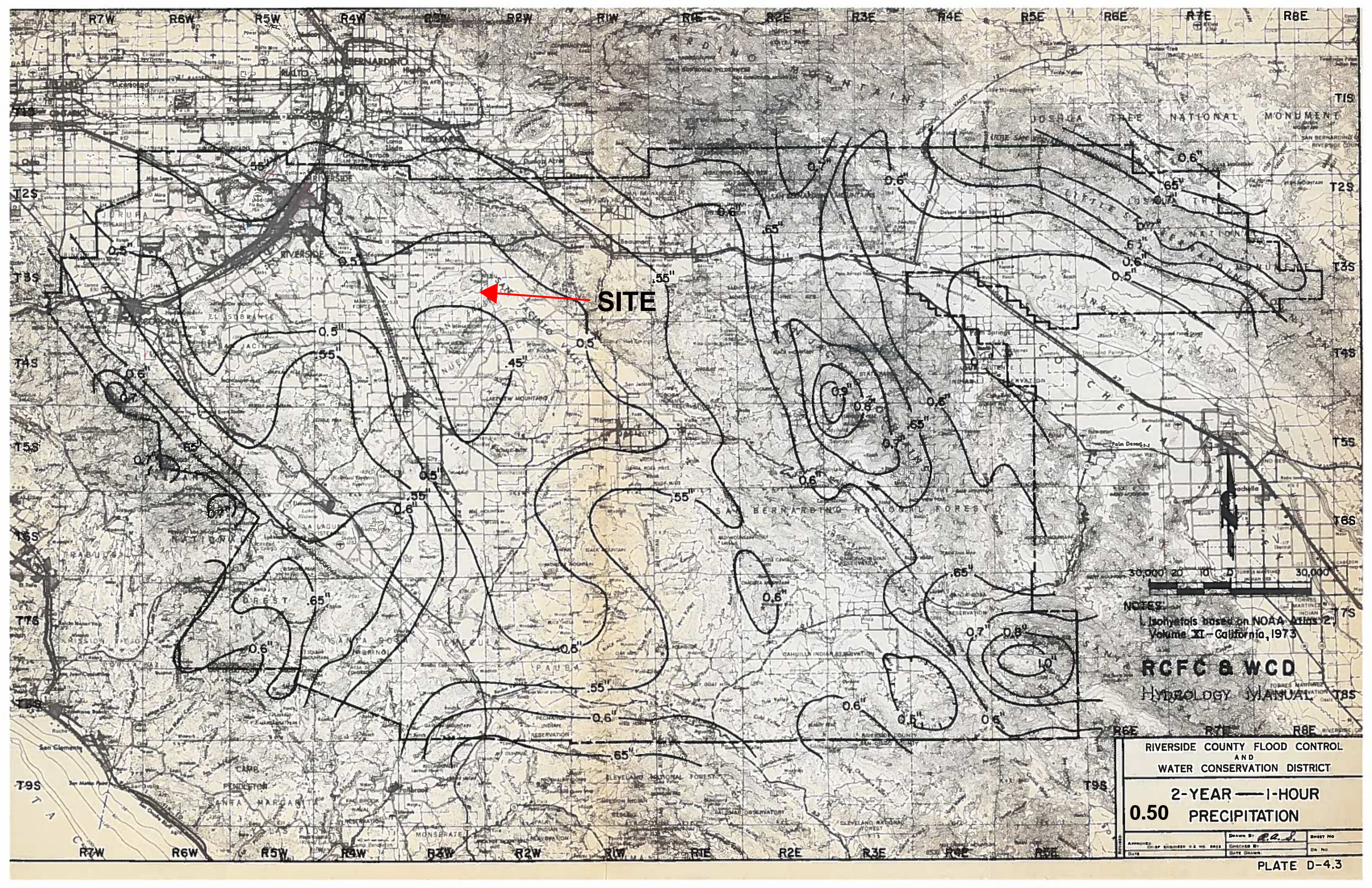
**LEGEND**

— SOILS GROUP BOUNDARY  
 A SOILS GROUP DESIGNATION

**RCFC & WCD**  
 HYDROLOGY MANUAL

0 FEET 5000

**HYDROLOGIC SOILS GROUP MAP**  
 FOR  
**B**  
**TYPE** **SUNNYMEAD**



**SITE**

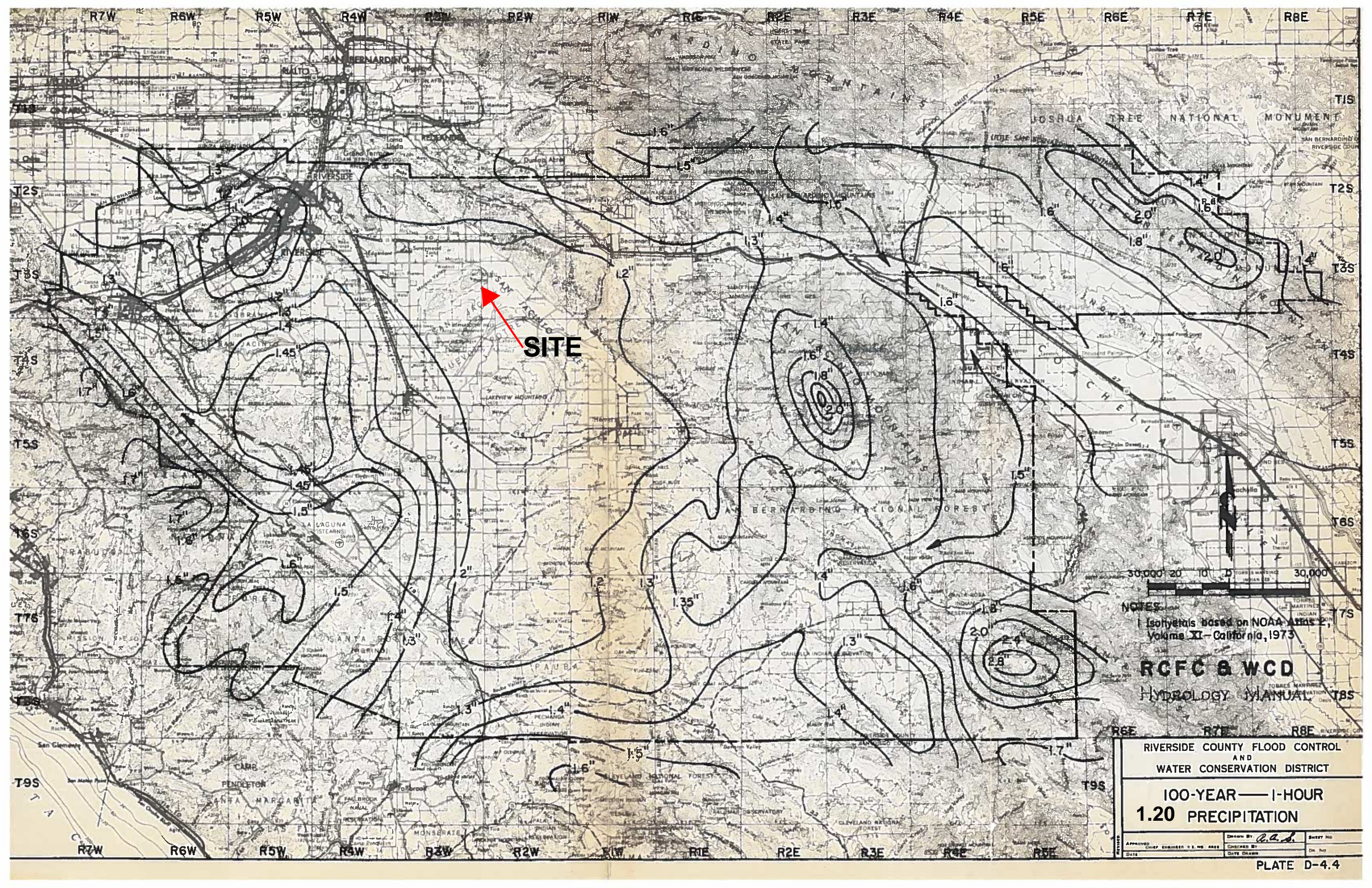
NOTES:  
 Isohyets based on NOAA Atlas 2,  
 Volume XI - California, 1973

**RCFC & WCD**  
 HYDROLOGY MANUAL

RIVERSIDE COUNTY FLOOD CONTROL  
 AND  
 WATER CONSERVATION DISTRICT

**2-YEAR — 1-HOUR  
 0.50 PRECIPITATION**

APPROVED	DATE	DESIGNED BY	DATE	DRAWN BY	DATE	SHEET NO.



**SITE**

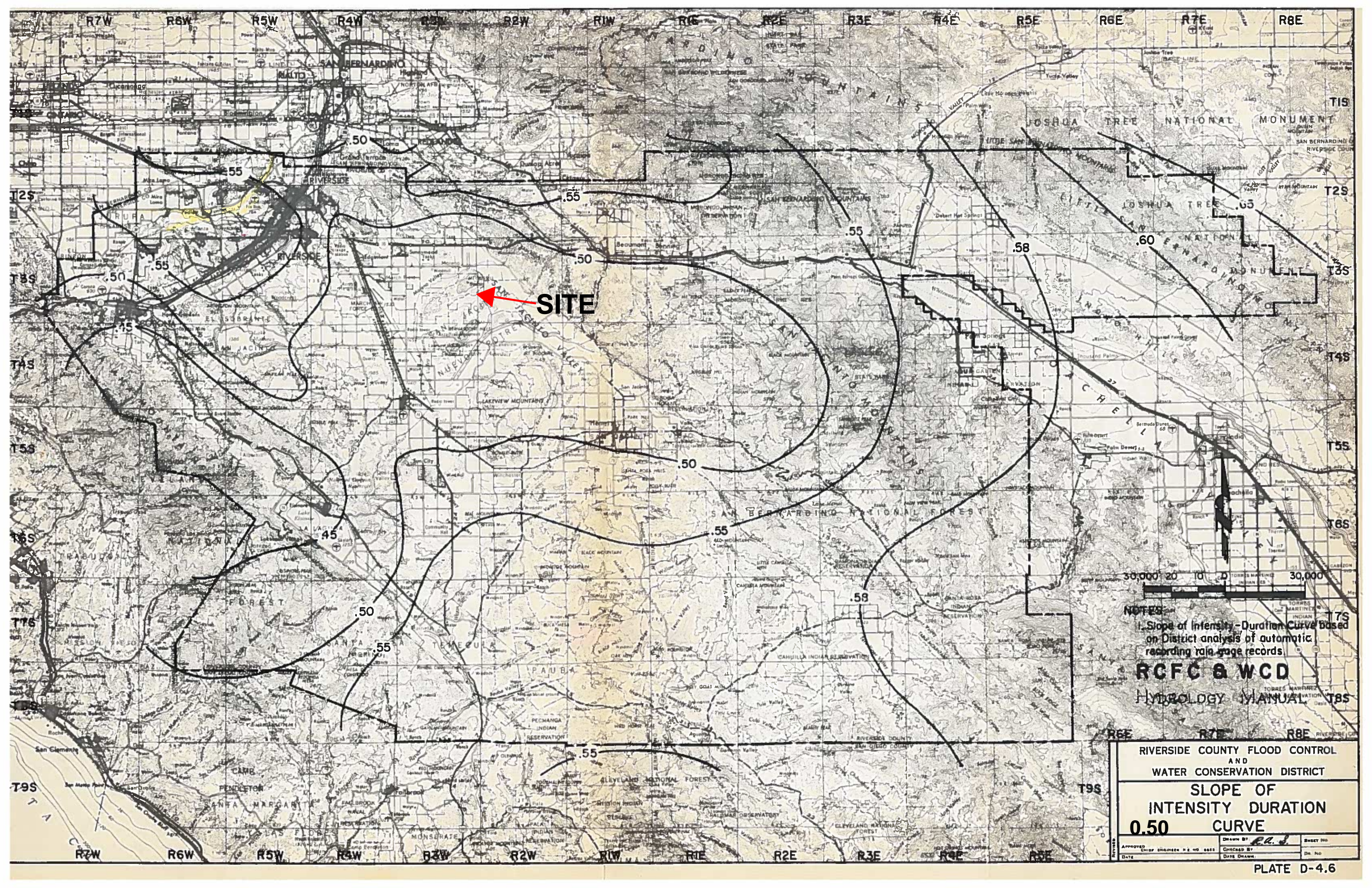
NOTES:  
 1. Isohyets based on NOAA Atlas 14, Volume XI - California, 1973

**RCFC & WCD**  
 HYDROLOGY MANUAL

RIVERSIDE COUNTY FLOOD CONTROL  
 AND  
 WATER CONSERVATION DISTRICT

**100-YEAR — 1-HOUR  
 1.20 PRECIPITATION**

APPROVED	CHIEF ENGINEER	DATE	DRAWN BY	DATE	SHEET NO.
			<i>R.A.S.</i>		



**SITE**

NOTES  
 1. Slope of Intensity-Duration Curve Based on District analysis of automatic recording rain gage records.

**RCFC & WCD**  
 HYDROLOGY MANUAL

RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT  
**SLOPE OF INTENSITY DURATION CURVE**  
**0.50**

APPROVED CHIEF ENGINEER R. E. NO. 6663	DRAWN BY C. J. J.	SHEET NO.
DATE	CHECKED BY	DR. NO.
	DATE DRAWN	